

Stress Analysis of FRP Composite Cylinder with Closed Ends

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Abstract: Composite cylinders made of a polymer matrix such as epoxy reinforced with glass or carbon fibers possess extremely high strength. Proper modeling of FRP composite cylinder is very essential for many applications. FRP composite cylinders are commonly used in the aerospace, automotive, marine and construction industries. The present work is to study the variation of stresses at the top end, middle and bottom end portions of a composite cylinder by varying the diameter to thickness ratio (S) and fiber angle (θ). The four layered angle ply ($\theta^0/-\theta^0/-\theta^0/\theta^0$) composite cylinder is considered for the present work and behavior of each portion (Top end, middle and Bottom end) is studied. For the present work composite cylinder is modeled in ANSYS and analysis was carried out using numerical software. It is found that the increment of stress takes place linearly with respect to D/t ratio due to reduction in thickness of the layer. The critical fiber angle is 45° to 60° as it offers high resistance against axial and circumferential deformation in middle and end portions.

Keywords: Composite Cylinder, Lamina, Fiber Angle, FEM, ANSYS

I. Introduction

The development of advanced fiber reinforced composite cylinders has been considered as the biggest technical revolution after the jet engine. FRP composites possess high strength and stiffness. In addition fatigue strength to weight ratio as well as fatigue damage tolerance of many composite laminates is excellent. Coefficient of thermal expansion for many FRP composites is much lower than those of metals. As such composite structures exhibit a better dimensional stability over a wide range of temperature variation. Damage of composite structures is usually in nature and can be detected only by sophisticated nondestructive testing. Because of their low maintenance cost and light weight, many structures are nowadays made of FRP composites. Spacecraft may have weight savings as much as 40 % if FRP composite structures are used. Therefore, the use of FRP composite materials is increasing compared to conventional materials. Adali et al [1] have derived three dimensional elastic conditions for axis symmetrical loading conditions for a multi-layered pressure vessel subjected to internal pressure. Roy and Tsai [2] found a simple design method for the stress analysis of a plane strain composite cylinder based on 3D elasticity. Starbuck [3] presented a closed form solution for the layer-by-layer stresses and strains based on the theory of anisotropic elasticity and plane deformation. Multi layered composite cylinders subjected to hygrothermal loading conditions were studied by Sayman [4]. Structural analysis of fiber reinforced pressure vessel have been investigated by Christos et al [5] for three different ply layers independently using computer code for simulation of damage and its growth due to internal pressure. Ahmadian and Bonakdar [6] investigated laminated hollow cylinders subjected to various loads and boundary conditions using 16 node cylindrical super element. Kranti [7] proved that a minimum of 100mm length is required to study the behavior of infinitely long FRP composite cylinder. E.V. Morozov [8] investigated the behavior of a thin walled composite cylinder when subjected to 2, 4 and 8 unit filament wound and also conducted the stress analysis for the cylinder. Rani Haj Ali et al [9] combined micromechanical and cohesive finite element modeling approach to predict the failure of a FRP composite under Mode-I and Mode-II loading conditions. A micromechanical constitutive model was used to capture the non-linear material response. For thick section composites, a mixed mode fracture failure criterion was proposed. S. Bhavya [10] conducted the failure analysis of an open end FRP composite cylinder and has observed that the stresses increase and load bearing capacity of cylinder decreases with increase in D/t Ratio. J. C. Velosa et al. [11] have studied composite pressure vessels for large scale market applications. These vessels consist on a thermoplastic liner wrapped with a filament winding glass fiber reinforced polymer matrix structure.

II. Problem Statement

The present work deals with the Stress analysis of the FRP composite cylinder with closed ends. A four layered ($\theta^0/-\theta^0/-\theta^0/\theta^0$) composite cylinder with semicircular ends is considered. A metal cap is provided in the ends for openings. The finite element models created in ANSYS software are validated and extended to evaluate the stresses at the top end, middle and bottom end portions of composite cylinder.

III. Modeling Of The Problem

3.1.1 Geometric Modeling

The geometry of the problem is:

Diameter of the cylinder = 100 mm,

Thickness of the cylinder = Dia. Of cylinder / S

(Where "S" is the diameter to thickness ratio whose value ranges from 5 to 100)

Stacking Sequence = $(\theta^0 / -\theta^0 / -\theta^0 / \theta^0)$

(Where " θ " is the fiber angle with respect to cylinder axis)

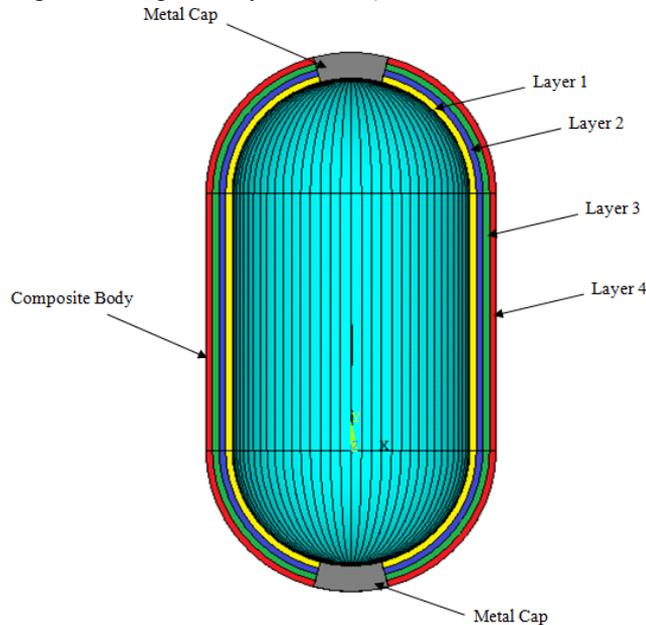


Fig 1. Composite Cylinder with four layers

3.1.2 Finite Element Modeling

Using ANSYS software the problem is modeled and the finite element model is generated using SOLID 191 element on four volumes corresponding to four layers of laminate structure. Solid 191 is a 20 node second order brick element having three degrees of freedom at each node and is suitable to incorporate orthotropic material properties. The finite element model is generated in ANSYS software for angle-ply laminate having stacking sequence of $(\theta^0 / -\theta^0 / -\theta^0 / \theta^0)$. The mesh refinement is carried out until the radial stresses at inner and outer surfaces of the cylinder closely matches with applied pressure and zero respectively. A separate coordinate system has been provided at the top end and bottom end for the analysis of semicircular caps.

3.1.3 Material Properties

In the present work carbon epoxy with the following properties are adopted

$E_1 = 147$ GPa	$\nu_{12} = 0.27$	$G_{12} = 7$ GPa
$E_2 = 10.3$ GPa	$\nu_{23} = 0.54$	$G_{23} = 3.7$ GPa
$E_3 = 10.3$ GPa	$\nu_{13} = 0.27$	$G_{13} = 7$ GPa

For Metal cap Steel with following properties are adopted

$E = 2e5$ MPA, $\nu = 0.3$

3.1.4 Boundary conditions and Loads

The symmetry line of the cylinder restricted to move in radial direction. Internal surface of the cylinder subjected to pressure of 1MPa

IV. Validity of the Present Analysis

Present finite element model is validated by verifying the radial, circumferential and axial stresses by applying isotropic material properties at middle location of the cylinder. It is observed that the finite element results are in close agreement with theoretical results. The theoretical results are obtained from lames equations.

	σ_r	σ_c	σ_a
Theoretical	-0.42525	4.47525	2.025
Ansys	-0.42145	4.5938	2.024
% Error	0.893592	2.64901	0.049383

V. Results and Discussions

The finite element model is generated in ANSYS software and the stresses are obtained. The results are taken for the following two cases.

1. Analysis of cylinder with various D/t ratio
2. Analysis of cylinder with various fiber angles.

VI. Effect of D/t Ratio

The variation of radial stress with respect to Diameter to thickness ratio (S) is plotted as shown in the figure 2 for top end, middle and bottom end portions of a FRP composite cylinder. It is observed that at middle portion the radial stress almost remains constant and the maximum stress is observed in the end portions of the composite cylinder because of curvature and the value of the maximum radial stress is observed to be 1.62 MPA.

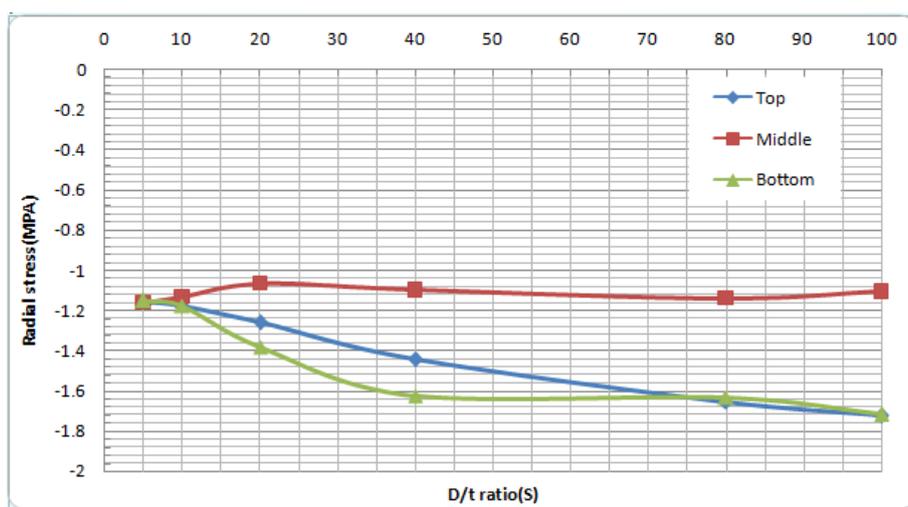


Fig 2. Variation of radial stress with respect to D/t Ratio(S).

The variation of circumferential stress with respect to Diameter to thickness ratio (S) is plotted as shown in the figure 3 for top end, middle and bottom end portions of a FRP composite cylinder. It is observed that circumferential increases linearly in all the three portions with increase in the d/t ratio. The maximum stress is observed in the top and bottom portions whose value is equal to 60MPA. The increase in stress takes place due to reduction in thickness of the layer.

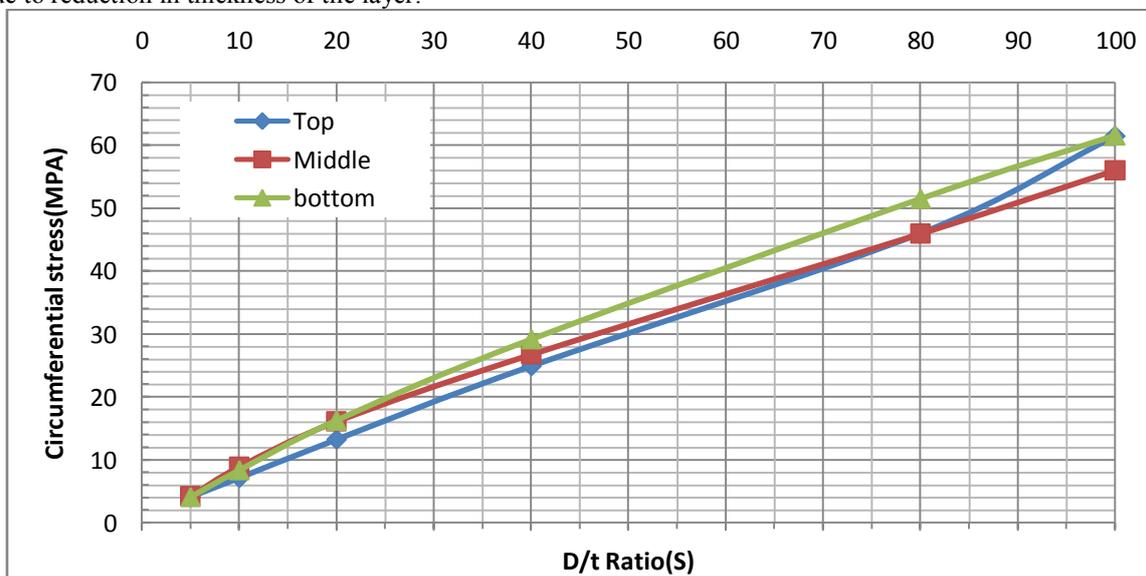


Fig 3. Variation of circumferential stress with respect to D/t Ratio(S)

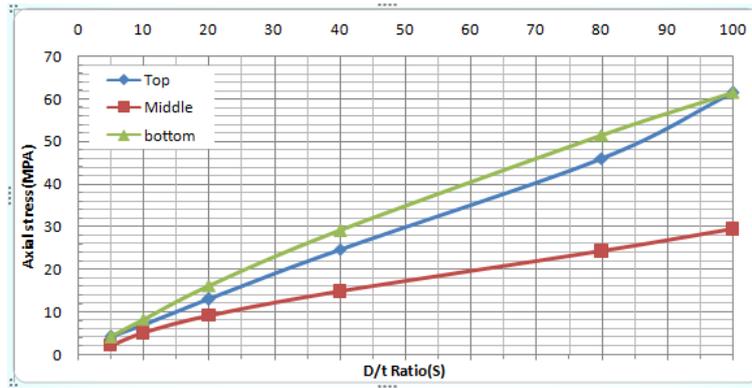


Fig 4. Variation of Axial stress with respect to D/t Ratio(S)

The variation of axial stress is shown with respect to D/t ratio is as shown in fig 4. It is observed that axial stress increases linearly in all the three portions with increase in the d/t ratio. Compared with middle portion in end portions stress increment is maximum due to curvature in geometry. The maximum stress obtained in the top and bottom end portion is equal to 61MPa.

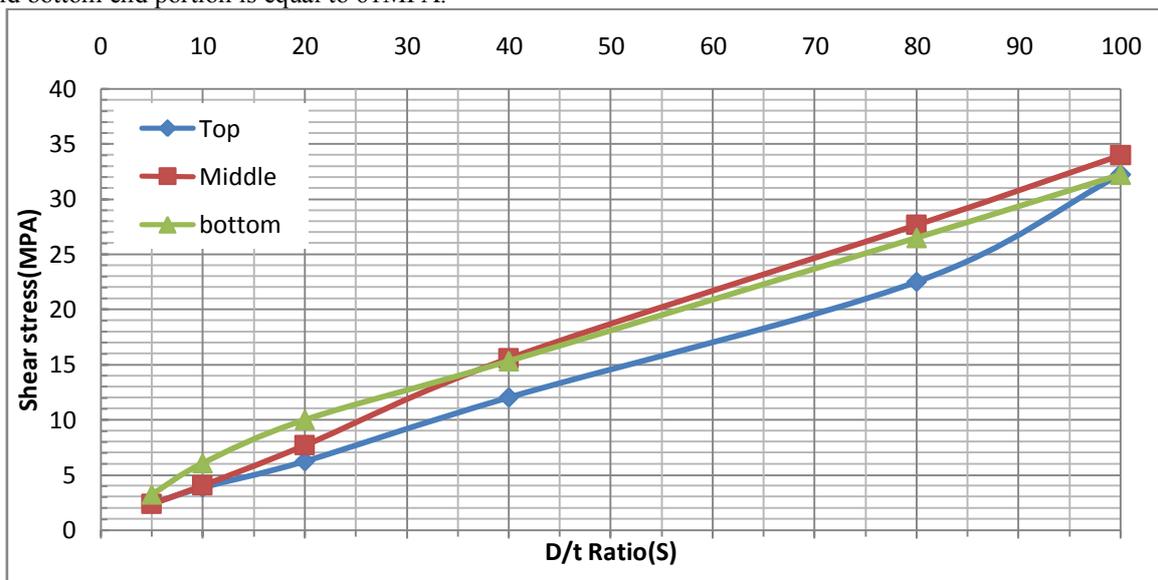


Fig 5. Variation of Shear Stress with respect to D/t Ratio.

It is observed that the shear stress ($\tau_{\theta z}$) goes on increasing with an increase in d/t ratio. All the three portions exhibit the same kind of behavior and the maximum value of stress at the d/t ratio of 100 is 32MPa.

VII. Effect of Fiber Angle

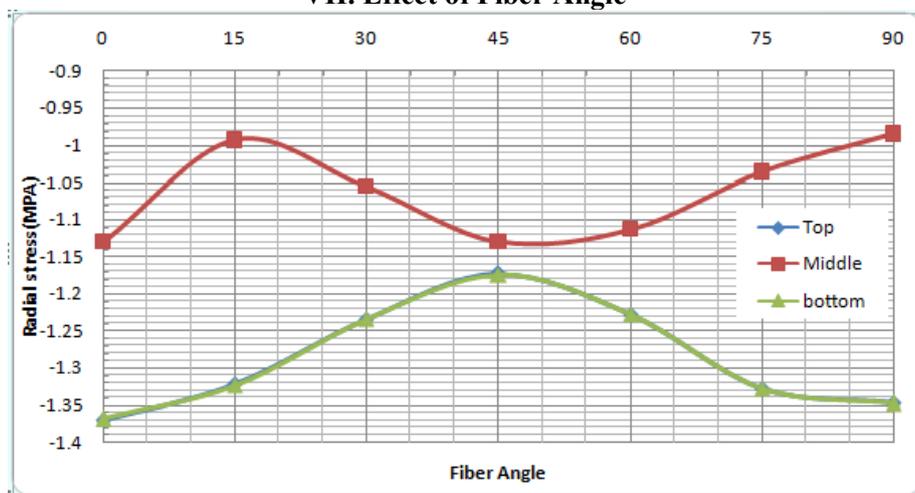


Fig 6. Variation of Radial stress with respect to Fiber Angle

The variation of radial stress with respect to fiber angle is as shown in fig 6. For the middle portion the critical portion where the maximum stress occurs are 15° fiber angle and 90° fiber angle. For the ends the maximum stress occurs at 45° fiber angle and hence it is considered as critical angle for the radial stress at ends. However the maximum value of stress 1.2 MPA occurs at ends compared to middle portion. So 45° is considered as safe fiber angle for both middle and end portions

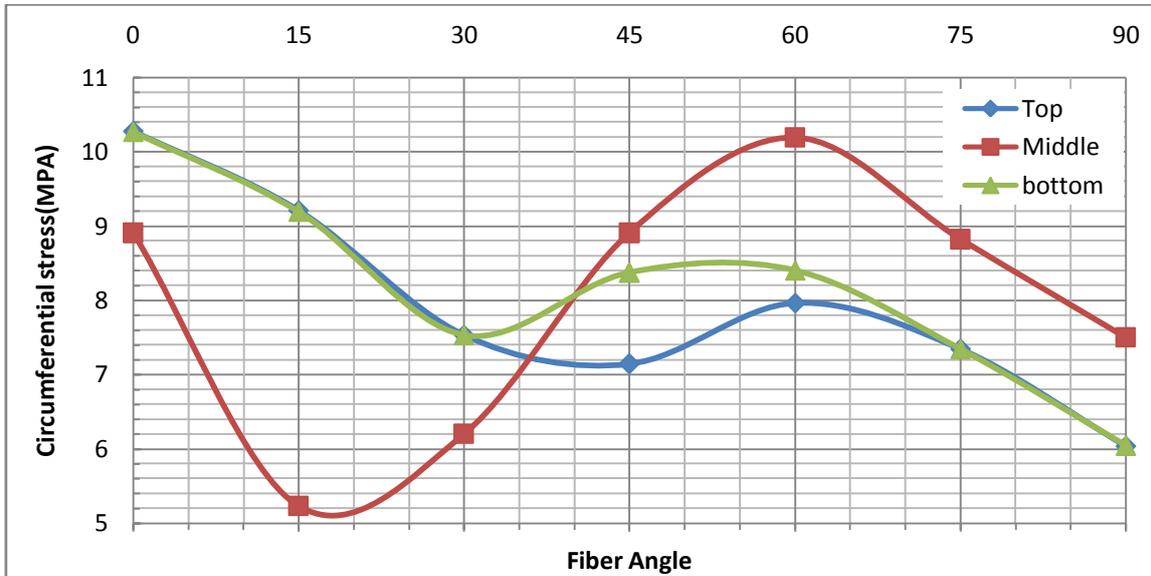


Fig 7. Variation of circumferential stress with respect to Fiber Angle

The variation of circumferential stress with respect to fiber angle is as shown in fig 7. It is observed that 60° is the critical angle for middle portion as the maximum amount of stress 10.2 MPA occurs here. At the ends the maximum stress predicted is 11 MPA. So below 45° fiber angle end portion will be considered as critical section. In the case of above 45° fiber angle middle portion will be the critical section due to high stress.

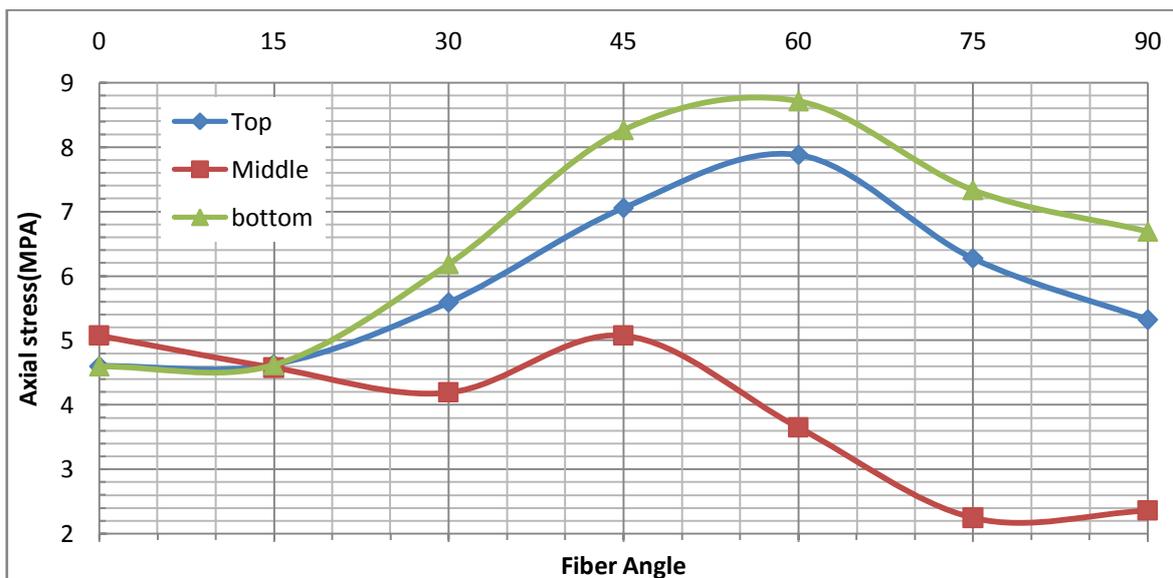


Fig 8 Variation of Axial stress with respect to Fiber Angle

The variation of axial stress with respect to fiber angle is as shown in fig 8. It is observed that all the three portions have uniform stress up to 15° fiber angle. In middle portion maximum stress occurs at 45° fiber angle. For the end portions maximum stress occurs at 60° fiber angle. This is due to high resistance offered against axial deformation at this fiber angle. So 45° to 60° will be treated as critical fiber angles.

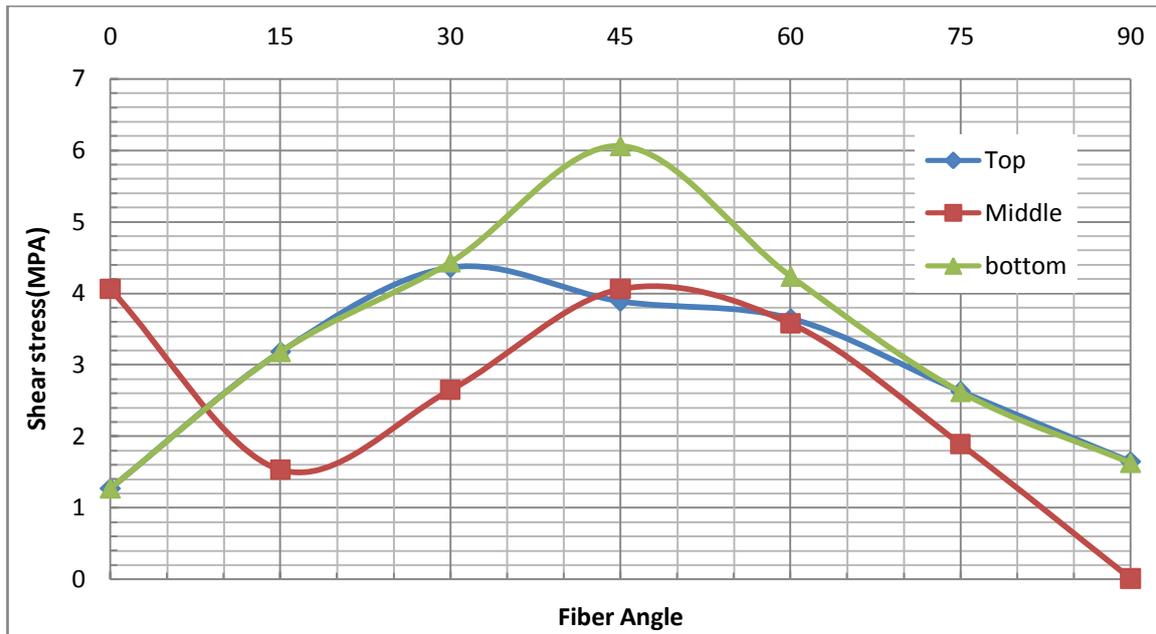


Fig 9 Variation of Shear stress with respect to Fiber Angle

The variation of shear stress ($\tau_{\theta z}$) with respect to fiber angle is shown in fig 9. The maximum stress obtained in all portions at of 45° fiber angle. This is due to high resistance offered against pressure loading in axial and circumferential direction. Therefore 45° is the critical fiber angle which influences shear stress for all the three portions.

VIII. Conclusions

A FRP composite cylinder with closed ends consisting of four layers is analyzed in the present work. Variation of stresses with respect to diameter to thickness (S) ratio and fiber angle have been presented. The stresses are increased with respect to diameter to thickness ratio due to reduction in thickness of the layer. Similar behavior is observed for middle and end portions. In the case of variation of stresses with respect to fiber angle, ends behave differently compared to middle portions. From the results it is concluded that the critical fiber angle is 45° to 60° as it offers high resistance against axial and circumferential deformation in middle and end portions.

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