Study of Fracture Behaviour of A Composite Laminate[0°/90°] with Circular Crack Subjected to Thermo-Mechanical Loading with Temperature Fall

V.V.Venu Madhav^a*, A.V.S.S.K.S. Gupta^b And P. Rakesh^c

^aDepartment of Mechanical Engineering, V. R. Siddhartha Engineering College, Vijayawada, Andhra Pradesh-520007, India

^bDepartment of Mechanical Engineering, JNTU College of Engineering, Hyderabad, Telengana-500085, India. ^cSr. Engineer, DesignTech Systems Ltd., APCOE, VRSEC, Andhra Pradesh-520007, India. Corresponding Author:- V.V.Venu Madhava

Abstract: There is an increased usage of advanced composite structures due to several inherent benefits that they offer in comparison with the monolithic materials. But the application of these materials is being limited by the fact that the knowledge about the crack propagation and strength behaviour under application of loads and environmental conditions is not extensive. So, undertaking research in this direction is still very much important. In this paper, a circular crack which is present in the middle of a composite laminate was modelled and then subjected to combined (temperature + pressure) loading conditions where the temperature was considered to be falling and pressure remaining constant to study the fracture behaviour. The fracture behaviour of the composite laminate was studied using the strain energy release rate (SERR) value calculated using Virtual crack closure technique (VCCT). The effect of the combined thermo-mechanical loading conditions on the SERR value in the 3 different modes of fracture with a circular crack located in the middle of the composite laminate was studied and the influence of these parameter was discussed in this paper.

Keywords: Thermo-Mechanical Loading, SERR, VCCT, Composites Fracture, FEA.

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I. Introduction

Due to the characteristics such as light weight, higher stiffness to weight ratio, high strength to weight ratios, the usage of advanced composites as a structural material has increased multiple folds in the 20th century. This is the main factor that has sparked interest in number of researchers for predicting their behavioural characteristics of these composite laminated materials. Fracture failures occur in composite laminates more often than anticipated. The ability to predict the facture behaviour of the laminate under different loading conditions is critical to avoid catastrophic failure of the composite materials. A lot of understanding is required on the crack propagation in different modes and mixed modes due to the application of the temperature loading and combined loading especially when the temperature is falling as these two conditions are most often endured by the composite laminates in operation in addition other factors.

Researchers have tried to predict the fracture behaviour of different functionally graded materials, composite laminates...etc., Jin et. al. [1] considered an edge crack in a multi-layered FGM stressed under the transient thermal loading. The material was assumed to be thermally non-homogenous material and they calculated thermal stress intensity factors(TSIF) of TiC/SiC FGM for various volume fractions. It had been noted that TSIF could be reduced or increased with respect to the FGM strip used Tic, SiC respectively. Rolfes et. al. [2] developed 2D elements for both steady state and transient problems; which were explicitly used for modelling laminated plates and cylindrical shells, that reduces the order of shape function. These elements have been verified with the help of different thermal lamination theories. Matsunaga. [3] presented a 2-D global higher order deformation theory for thermal buckling analysis of angle-ply laminated composite and sandwich plates. He used the virtual energy method to derive the governing equations which takes the shear and normal stresses in to consideration. The variation the displacement continuity functions for the 3-D layer wise theory and global higher order theories applied for thermal buckling of the angle ply and sandwich panels were explained. Tsang et. al. [4] used 2-D fractal elements in analysing the cracks on thermo-elastic problems. Transformation functions were analytically established to check thermal stress intensity factor with respect to thermal loading. Kerezsi et.al. [5] through experimental investigation exposed the specimen for continuous 1-D thermal shocks, so to find out how the growth of crack develops and the method to analyse it. for predicting accurate results, they developed a two-stage crack growth model which also includes the effect of environment on the crack growth where the model was just true for carbon steel at below operating temperatures of creep range. The two stages of model correspond to the high strain fatigue region and linear elastic fracture mechanics respectively. Herrmann et.al. [6] considered an interfacial crack with a contact zone with thermal problem as a Dirichlet-Riemann boundary value problem and solved it. They derived analytical formulations to determine the real contact zone length. They found that the real contact zone length and its corresponding stress intensity factors depends on normal shear loading and heat flux. Panda et.al. [7] assumed linear elasticity for mechanical loading which super imposed the thermal stresses where strain energy rates were calculated at delamination front. They concluded that the anisotropy and heterogeneity nature of the composite forges to be a cause for mixed mode of interlinear fracture at delamination front. Gardinet.al. [8] analytically modelled the crack shape for a thermal cyclic loading induced with a thermal gradient in the specimen's thickness using stress intensity factors, weight functions and Paris law. The influence of thermal gradient on crack propagation were understood by comparing their analytical solution with FEM and experimental results. Shahani et.al. [9] first analytically derived the steady state solution to thermo-elastic problem and later use weighted function method to know the stress intensity factors to determine from where semi elliptical crack initiates. Pradhan et.al.[10] discussed the manufacturing defects that causes inter laminar elliptical delamination's to forego crack growth influenced by ply angle and thermo-elastic loading. Bhalla et.al.[11] describes about the energy consumed in the crack growth and about the material damage. They used infrared cameras to study the crack growth by analysing thermal images. by calculating the energy flux, crack growth can be studied. Tang [12] studied a crack line subjected to thermo-mechanical loading in an infinite plate. To facilitate solution for the problem, complex function method was integrated with thermo-elastic theory. Only mode I stress intensity factor was found to be effective and the heat flux along the vertical direction to the crack line has no effect on the thermal stress intensity factor. So, strain energy density factor theory had been effectively used to calculate applied failure stresses. It was noted that the direction of the heat flow has an influence on the crack growth whether it may be positive or negative. Many other references regarding the composite materials, facture and FEM analysis of composite material as have been referenced from [13-30].

II. Fea Work

2.1. Problem Description:

A composite laminate containing a circular hole & a virtual crack at its centre was considered. The Effect of combined loading (temp fall + pressure) on the on the crack propagation was studied. From the results obtained through this work, conclusions were taken and presented in this paper.

2.2 Geometry

The geometry of the composite laminate was taken as 100 X 100 X 5 mm in length, width and thickness dimensions. The thickness of the laminate was divided into 4 laminas with a thickness of 1.25mm for each layer. A symmetric layup sequences of $[\theta, -\theta, -\theta, \theta]$ was considered for modelling the fiber angles of the laminate with θ taking the values of 0°,90° in different configurations. A circular hole of 40mm diameter is placed at the centre of the composite laminate and a virtual circular crack of 0.22mm diameter was modelled at exact mid plane of the composite laminate. The geometry of the composite laminate is shown in the fig.1 and the geometry of the edge crack is shown in the fig.2. Different configuration used for the analysis are shown in the fig.3.



Fig.1: Geometry of the Composite Laminate



Fig.2: Geometry of the Virtual Crack



Fig.3: Different configurations of the Angle ply composite laminate

2.3. FE Model

The above-mentioned geometry was converted in to finite element model using the process of meshing. For this purpose, the solid 20 node 186 elements with suitable refinement and mesh settings was used. It is an element which is suitable for modelling of both homogeneous solids and also layered solids effectively. In our work the element was used to mesh a layered solid. Fig.4 shows the FEA element used for meshing the composite geometry.



Fig.4: 20 Node 186 Solid Element used for Meshing

2.4 Material Properties

As4 carbon fiber embedded inside the 3501-6 epoxy was the lamina material that was considered for the modelling the composite. The material properties were taken from the textbook of I.M.Daniel& Ori ish [30]. Once the material properties of the lamina with 0° fiber angle were taken from the reference, these properties of the lamina were used to find out the properties of the lamina with 90° using a simple MATLAB code. Table.1 shows the properties of the AS4/3501-6 Carbon/Epoxy lamina.

			<u> </u>	erties taken	for FEA		Table.1: Material Properties taken for FEA bon Composite Properties					
As4/3501-6 Epoxy carbon Composite Properties												
E ₁₁ (Gpa)	E ₂₂ (Gpa)	E ₃₃ (Gpa)	G12(Gpa)	G ₂₃ (Gpa)	G ₁₃ (Gpa)	v ₁₂	v ₂₃	v ₁₃				
147	10.3	10.3	7.0	3.48	7.0	0.27	0.51	0.27				
		1 (10⁻⁶/ºC) 1.9	<u>α</u> ₂ = 27	$= \alpha_3 (10^{-6}/^{\circ}C)$		-						

2.5 Boundary & Loading conditions:

Simply supported boundary conditions were place at the four edges of the lamina using the displacement constraints in the Ansys Software. Thermal loading was considered, different temperature starting from -30 $^{\circ}$ C to -180 $^{\circ}$ C with a step size of 50 $^{\circ}$ C were applied on the composite laminate in combination of a

pressure load of 5 Mpa applied to the top face of the laminate in the downward direction in addition to the earlier stated thermal loading. Fig.5represents the boundary conditions considered for the present work



Fig.5: Boundary Conditions applied for the composite laminate

2.6 Validation of FE Model:

Validation of the FE model was conducted using the results taken from V.V. Venumadhav et al. [13]. Different crack lengths were taken and the SERR values obtained from our FE model were validated against the reference. Table.2 shows the results obtained from validating the FE model.

Virtual Crack Length (mm)	Present SERR (KJ/m ²)	Reference SERR (KJ/m ²)	% of Error	
5	12.64	12.35	2.35	
3	11.36	11.22	1.22	
2	10.81	10.64	1.64	
1	10.16	10.05	1.05	
0.5	10.23	9.94	2.94	

From the results obtained from the table.2, it can be stated that the percentage of error between the FEM values and the reference values is very low. From this we can say that our FEM model has been verified.

III. Results

Effect of Combined (Thermal + Mechanical) Loading:

The variation on the SERR values for different fracture modes for the circular hole & crack that is located at the middle of the composite laminate due to the application of the combined loading for different fiber angles of the composite are shown in the fig. 6,7,8.



Fig.6: SERR vs Temperature (combined) for different fiber angles for Fracture Mode-I

From the figure 6, it can be observed that as the temperature is decreasing and the pressure load remaining the same, there is no evident change that was observed in the SERR value. This trend was observed in the case of all the angle ply composite laminates with the different fiber angles. But as the fiber angle is

increasing the SERR value was decreasing, but that change also minimal. So, there is no evident effect of temperature fall and a slight effect of the fiber angles on SERR value is observed in fracture mode -I (G_I), for the laminate with the circular hole & crack at the middle of the laminate subjected to combined (temp fall + pressure) loading.



Fig.7: SERR vs Temperature (combined) for different fiber angles for Fracture Mode-II

From the figure 7, it can be observed that as the temperature is decreasing and the pressure load remaining the same, the SERR value is also increasing. This trend was observed in the case of all the angle ply composite laminates with the different fiber angles. As the fiber angle is increasing the SERR value is increasing, but that change also minimal. The maximum effect of the fiber angle was observed at lower temperatures in the case of the combined loading. So, there is an evident effect of temperature fall and a slight effect of the fiber angles on SERR value is observed in fracture mode -II (G_{II}), for the laminate with the circular hole &crack at the middle of the laminate subjected to combined (temp fall + pressure) loading.



Fig.8: SERR vs Temperature (combined) for different fiber angles for Fracture Mode-III

From the figure 8, it can be observed that as the temperature is decreasing and the pressure load remaining the same, there is no evident change that was observed in the SERR value. This trend was observed in the case of all the angle ply composite laminates with the different fiber angles. But as the fiber angle is increasing the SERR value was increasing, with a considerable change in value. So, there is no evident effect of temperature fall and a great effect of the fiber angles on SERR value is observed in fracture mode -III (G_{III}), for the laminate with the circular hole & crack at the middle of the laminate subjected to combined (temp fall + pressure) loading.

The variation on the SERR values for different mixed fracture modes for the circular hole & crack that is located at the middle of the composite laminate due to the application of the combined loading for different fiber angles of the composite are shown in the fig. 9,10,11.



Fig.9: SERR vs Temperature (combined) for different fiber angles for mixed fracture Mode-I

From the figure 9, it can be observed that as the temperature is decreasing and the pressure load remaining the same, The SERR values are decreasing. This trend was observed in the case of all the angle ply composite laminates with the different fiber angles. But as the fiber angle is increasing the SERR value was decreasing. The profound effect on the combined loading is evident in the case of 0° fiber angle lamina-based composite. The maximum effect of the fiber angle was observed at higher temperatures in the case of the combined loading. So, there is evident effect of temperature fall and the fiber angles on SERR value is observed in mixed fracture mode -I (G_I/G_T), for the laminate with the circular hole & crack at the middle of the laminate subjected to combined (temp fall + pressure) loading.



Fig.10: SERR vs Temperature (combined) for different fiber angles for mixed fracture Mode-II

From the figure 10, it can be observed that as the temperature is decreasing and the pressure load remaining the same, the SERR values are increasing. This trend was observed in the case of all the angle ply composite laminates with the different fiber angles. But as the fiber angle is increasing the SERR value was decreasing. The profound effect on the combined loading is evident in the case of 0° fiber angle lamina-based composite. The maximum effect of the fiber angle was observed at lower temperatures in the case of the combined loading. So, there is evident effect of temperature fall and the fiber angles on SERR value is observed in mixed fracture mode -II (G_{T}), for the laminate with the circular hole & crack at the middle of the laminate subjected to combined (temp fall + pressure) loading.



Fig.11: SERR vs Temperature (combined) for different fiber angles for mixed fracture Mode-III

From the figure 11, it can be observed that as the temperature is decreasing and the pressure load remaining the same, The SERR values are decreasing. This trend was observed in the case of all the angle ply composite laminates with the different fiber angles. But as the fiber angle is increasing the SERR value was increasing. The profound effect on the combined loading is evident in the case of 0° fiber angle lamina-based composite. The maximum effect of the fiber angle was observed at higher temperatures in the case of the combined loading. So, there is evident effect of temperature fall and the fiber angles on SERR value is observed in mixed fracture mode -III (G_{III}/G_T), for the laminate with the circular hole & crack at the middle of the laminate subjected to combined (temp fall + pressure) loading.

IV. Conclusions

Inter laminar fracture analysis of a four-layered angle-ply symmetric simply supported laminate with a circular hole and a crack at the centre of the plate in middle interface was modelled and subjected to uniform transverse pressure and temperature fall. The crack propagation was studied using Virtual Crack Closure Technique using the technique of finite element analysis. The SERRs in principal modes with respect to change in size of the delamination are evaluated.

- The SERR in mode-II is high compared to all the three principle modes in Thermo-mechanical fall loading.
- Mixed mode fracture behaviour is observed.
- In Mode-I SERR is high for fiber angle $\theta = 0^0$ in Thermo-mechanical fall loads.
- In Mode-II SERR is high for fiber angle $\theta = 90^{\circ}$ in Thermo-mechanical fall loads.
- In Mode-III SERR is high for fiber angle $\theta = 90^{\circ}$ in Thermo-mechanical fall loads.
- In mixed Mode for Mode-I SERR is high for fiber angle $\theta = 0^0$ in Thermo-mechanical fall loads.
- In mixed Mode for mode-II SERR is high for fiber angle $\theta = 0^0$ in Thermo-mechanical fall loads.
- In mixed Mode for mode-III SERR is high for fiber angle $\theta = 90^{\circ}$ in Thermo-mechanical fall loads.

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