# Ultrasonic Studies in the Binary Mixtures of Dimethyl Carbonate with Some Aliphatic Esters

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#### Abstract

The binary mixes Di Methyl Carbonate (DMC) + Methyl Acetate (MA), + Ethyl Acetate (EA), and + Butyl Acetate (BA) were measured for ultrasonic velocity (U), density ( $\rho$ ), and viscosity ( $\eta$ ) at four different temperatures (303.15-318.15K) covering the whole composition range. Deviations in adiabatic compressibility and viscosity, as well as excess values of molar volume, intermolecular free length, and relaxation time, were computed from the experimental data. To find binary constants and the standard deviation ( $\sigma$ ) between the estimated and experimental values, the Redlich-Kister polynomial equation has been fitted to the values of  $V^{\rm E}$ ,  $\Delta \beta_{\rm ad}$ ,  $L_{\rm f}^{\rm E}$ ,  $\Delta \eta$ .

Keywords: Di methyl carbonate, Densities, Speed of sound, Viscosity Compressibilities, Molar volumes, Inter Molecular Free Lengths.

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## I. Introduction

In the majority of engineering computations, where fluid flow or mixing plays a significant role in numerous real-world issues pertaining to mass transport applications, the physical characteristics of liquid mixes are necessary. DMC has a dipole moment of 0.90 D and is a polar, aprotic solvent. DMC is primarily utilized as an intermediate in the synthesis of different polymers and in the electrolytes of lithium-ion batteries, which are anticipated to be crucial for energy storage, as well as in the manufacturing of biodiesel and building materials like paints and cleaning and degreasing agents. On the other side, esters are used as plasticizers in the polymer processing industry to promote thermoplastic behaviour [1-3]. It is crucial to comprehend how DMC mixes with esters because this knowledge may be useful in a variety of engineering fields. At 303.15, 308.15, and 313.15 K, we present the density, viscosity, and sound speed findings for the binary mixes of DMC with methyl acetate, ethyl acetate, n-butyl acetate, and n-butyl acetate across the whole composition range. This information has been used to calculate the excess molar volume, viscosity deviations, sound speed deviations, adiabatic compressibility deviation, acoustic impedance, and excess Gibbs free energy of activation of viscous flow. To determine the binary coefficients and standard deviation, these findings were fitted to the Redlich-Kister polynomial equation using a multiparametric nonlinear regression analysis technique.

## **II. Experimental Techniques**

### a) Measurement of Velocity

The formula  $U=\lambda f$  can be used to calculate the ultrasonic velocity. The frequency of the generator employed in the investigation is 2 MHz. To get the high frequency generator's anode current meter to read its maximum, a micrometer screw and a lot of work were required. While adjusting the micrometer screw for n peaks, we should note how many times the anode current was at its highest.

 $d = n\lambda/2$ 

Multiplying the displacement of the reflector by 20 peaks by 100 makes it easy to determine the speed in meters per second. Since the distance 'd' can be determined with a micrometer to an accuracy of 0.01 mm or more, the quality of the distance measurement largely determines the velocity's precision.

#### b) Measurements of Density

In the current investigation, a specific gravity bottle with a 5ml volume was used to test the density ( $\rho$ ) for pure liquids and all liquid combinations at various temperatures between 303.15K and 318.15K with a 5K interval. One of the factors utilized to assess the liquids' purity was their density. To achieve thermal equilibrium, the specific gravity bottle was placed in the thermostat for fifteen minutes. When they reach room temperature, they are taken out of the thermostat and weighed. There is a 0.5 mg margin of error in the density readings.

#### c) Measurements of Viscosity

At 303.15, 308.15, 313.15, and 318.15K, the viscosity was measured using a 0.55mm diameter Ubbelohde capillary viscometer that was calibrated using double-distilled water. The viscometer is calibrated using pure water, and the liquid is allowed to stand in a thermostatic water bath for about half an hour to minimize temperature swings. The precision of the viscosity measurements is 0.005 mPas.

#### **III. Theoretical Considerations**

i) Molar volume

$$V = M/\rho 3.1$$

ii). Excess Volume (VE)

$$V^{E} = V - (V_{1}X_{1} + V_{2}X_{2})$$
3.2

where  $X_1$  indicates the mole fractions of common compound and  $X_2$  indicates the molefraction of sub compound and  $V_1$  &  $V_2$  are the mean molar volumes respectively.

iii). Adiabatic Compressibility (β<sub>ad</sub>)

$$\beta_{\rm ad} = 1/\rho U^2 \qquad 3.3$$

iv). Deviation in Adiabatic compressibility ( $\Delta \beta_{ad}$ )

$$\Delta \beta_{ad} = \beta_{ad} - (\beta_{ad1} X_1 + \beta_{ad2} X_2) \qquad 3.4$$

where pure liquids' adiabatic compressibilities are indicated as  $\beta_{ad1}$  and  $\beta_{ad2}$ .

v). Intermolecular free length (L<sub>f</sub>)

$$L_f = K (\beta_{ad})^{1/2}$$
 3.5

Jacobson constant is indicated as K.

vi). Excess Intermolecular free length (L<sub>f</sub>)

$$L_f^E = L_f - (L_{f1}X_1 + L_{f2}X_2)$$
 3.6

pure liquids' intermolecular free length are  $L_{\rm fl}$  and  $L_{\rm f2}$  respectively

vii). Deviation in Viscosity ( $\Delta \eta$ )

The equation for deviation in viscosity is

$$\Delta \eta = \eta_{\text{mix}} - (X_1 \eta_1 + X_2 \eta_2)$$
 3.7

The liquid mixture and the pure liquids' viscosities are indicated as  $\eta_{mix}$ ,  $\eta_1$  and  $\eta_2$  are respectively.

The excess/deviation values of  $\Delta\beta_{ad}$ ,  $V^{E}$ ,  $\Delta\eta$ ,  $L_{f}^{E}$ , were least squares fitted to the Redlich – Kister type polynomial<sup>4</sup>

$$Y^{E} = X(1-X)\sum_{i=1}^{n} A_{i}(1-2X)^{i-1}$$
3.8

The coefficients of  $A_i$  in the above equation along with the standard deviation ( $Y^E$ ) are given in Tables. These coefficients are the adjustable parameters to get best - fit values of  $Y^E$  which are indicated in the table along with standard deviations ( $Y^E$ ) calculated by using the following relation

$$\sigma Y^{E} = \sum \left[ \frac{\left[ Y_{exp}^{E} - Y_{cal}^{E} \right]^{2}}{m-n} \right]^{1/2}$$
3.9

## **Theoretical Velocities**

Nomoto[5] developed the following ratio for liquid mixes assuming the additivity of molar sound velocity (R) and no volume change upon mixing

$$U_{N} = \left[\frac{X_{1}R_{1} + X_{2}R_{2}}{X_{1}V_{1} + X_{2}V_{2}}\right]^{3}$$
3.10

According to Blandamer and Waddington's [6] assumptions, the ideal mixing theory put forth by Van Dael and Vangeel [7] yields the following relation for ultrasonic velocity in liquid mixtures:

$$\frac{1}{\left[X_{1}M_{1} + X_{2}M_{2}\right]\left[U_{imx}\right]^{2}} = \frac{X_{1}}{M_{1}U_{1}^{2}} + \frac{X_{2}}{M_{2}U_{2}^{2}}$$
3.11

where  $U_{imx}$  is the liquid mixture's optimal ultrasonic mixing velocity. Ultrasonic velocity in species is represented by  $U_1$  and  $U_2$ .

Impedance Relation

Using the specific acoustic impedance of the pure liquids, the ultrasonic speed in the liquid mixtures is determined using the following relation[8]

$$U_{Imp} = \frac{\sum X_i Z_i}{\sum X_i \rho_i}$$
3.12

Where  $X_i$ s the molefraction,  $Z_i$  acoustic impedance and  $\rho_i$  is the density

Using the ratio of the temperature coefficient of speed and expansion coefficient, Rao[9] derived a formula for ultrasonic speed  $(U_R)$  given by

$$U_{R} = \left\lfloor \frac{R}{V} \right\rfloor$$
 3.13

where V is the molar volume and R is called Rao's constant or molar sound speed, which is constant for a liquid at a temperature. Junjie [10] assumed that the ultrasonic speed of the mixture depends on the mole fraction, molecular weight and density of the mixture. Junjie's relation is given by

$$U_{J} = \frac{\left[\frac{X_{1}M_{1}}{\rho_{1}} + \frac{X_{2}M_{2}}{\rho_{2}}\right]}{\left[X_{1}M_{1} + X_{2}M_{2}\right]^{1/2} \left[\frac{X_{1}M_{1}}{\rho_{1}U_{1}^{2}} + \frac{X_{1}M_{1}}{\rho_{1}U_{1}^{2}}\right]^{1/2}}$$
3.14

#### ix Chi-square test for goodness of fit

As indicated by Karl Pearson [11], Chi-square value is evaluated for the binary liquid mixtures under study utilizing the formula

$$\chi^2 = \frac{\left[U_{\text{obs}} - U_{\text{Cal}}\right]^2}{U_{\text{Cal}}}$$
3.1

where n is the number of data used, and U (obs) = experimental values of ultrasonic velocities U(cal) = computed values of ultrasonic velocities

## x Relative Percentage Error

The Average percentage error is calculated by utilizing the relation

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$$APE = \frac{1}{n} \sum \left[ \frac{U_{obs} - U_{cal}}{U_{obs}} \right] \times 100$$
3.16

#### xi Molecular Association

The degree of intermolecular interaction or molecular association is given by

$$\alpha = \frac{U_{exp}^2}{U_{imx}^2} - 1$$
3.17

## IV. Solvent purification

Because the purity of the liquid affects the accuracy and precision of the results, it is imperative to utilize the purest components available. When creating several purification methods, which are detailed in the literature, the type and functional groups of the compounds were taken into account [12,13].

Table-1: Literature Data in comparison with experimental data at 303.15K

Liquid	Density(ρ) Kg/m³		Velocity of U Sound(U		Viscosity(η) cP		
	Exptl	Lit	Exptl	Lit	Exptl	Lit	
DMC	1.0562	1.0567114	1175.3	117714	0.549	0.54914	
MA	0.9206	0.920115	1106	1106.515	0.372	0.351415	
EA	0.8885	0.888415	1117.3	1122.815	0.382	0.399515	
BA	0.8716	0.871215	1165.2	1176.415	0.643	0.640715	

## V. Results & Discussion

Tables 2, summarize excess characteristics of DMC with methyl, ethyl, and n-butyl acetate calculated by using the values of density, ultrasonic velocity, viscosity, andat temperatures ranging from 303.15 to 318.15K. Table 3 shows the values of parameters  $A_0$ ,  $A_1$ ,  $A_2$ ,  $A_3$ , and  $A_4$  derived by least squares analysis, along with their standard deviation.

Figs 1(a), 1(b) and 1(c) illustrate the relationship between excess volume ( $V^E$ ) and DMC mole fraction at various temperatures. The main causes of volume expansion, or positive  $V^E$  values, are

- (i) Chemical interactions between constituent molecules, such as the creation of H-bonds.
- (ii) Association through weaker physical forces, such as dipolar force or other similar factors.
- (iii) Molecules from one component are accommodated in the interstitial places of the other's structural network.

The strength of unlike molecular interactions in a solution can be assessed by the sign and magnitude of V<sup>E</sup>. V<sup>E</sup> values are negative across all three systems. However, methyl acetate has significantly higher negative V<sup>E</sup> values compared to other esters. The lower size of methyl acetate molecules in the DMC dipole network suggests interstitial accommodation. The negative V<sup>E</sup> values at higher temperatures suggest the interstitial accommodation of methyl acetate molecules [16].

DMC with aliphatic esters have algebraic V<sup>E</sup> values about 303.15K followed the order:

#### MA>EA>BA

Volume expansion is caused by the breaking up of molecular clumps or dipolar molecules, as well as dispersion forces between molecules.

The sign of a system's V<sup>E</sup> is determined by the relative expansion and contraction of the two liquids during mixing. Previous studies reported similar results [17].

The development of hydrogen bonds and dipole-dipole interactions between hetero molecules can significantly impact the system's compressibility. The differences in adiabatic compressibility can be explained by the following reasons.

- a) Differences in size and shape of component molecules reduce velocity and increase compressibility.
- b) Dipole-dipole interaction or hydrogen bonding between molecules leads to increased sound velocity and decreased compressibility.

The actual deviation is determined by the resulting effect. Figures 1(b), 2(b) and 2(c) show negative deviations in adiabatic compressibilities over DMC mole fractions, showing significant interactions between molecules.

 $\Delta\beta_{ad}$  values are consistently negative across all compositions and intensify at increasing temperatures. The structure of homologous series of esters has a significant impact on adiabatic compressibility. Figures 1(b), 2(b) and 2(c) show that when the ester chain length decreases, the  $\Delta\beta_{ad}$  values become increasingly negative.

In this investigation, the behavior of  $V^E$  and  $\Delta\beta_{ad}$  are comparable. The sign of  $\Delta\beta_{ad}$  supports the postulates used to understand the excess molar volume sign. Negative  $V^E$  and  $\Delta\beta_{ad}$  values may be caused by dipole-dipole and dipole-induced dipole interactions. [15-18] that improve the solvent structure of the mixture, hence lowering  $V^E$  and  $\Delta\beta_{ad}$ .

Table 2: Excess/deviation values of calculated thermodynamic parameters for DMC + MA, EA and BA systems at 303.15, 308.15, 313.15 and 318.15K

_	systems at 303.15, 308.15, 313.15 and 318.15K													
	DMC+Methyl Acetate DMC+Ethyl Acetate							DMC+Butyl Acetate						
$X_1$	ad	VE	$(L_f^E)$	( )	$X_1$	ad	VE	$(L_f^E)$	( )	$X_1$	ad	VE	$(L_f^E)$	( )
							303.15K							
0.0000	0.0000	0.0000		0.0000		0.0000	0.0000		0.0000		0.0000	0.0000	0.0000	0.0000
0.0949	-4.5347	-0.2162		0.3050		-3.8711	-0.1754		0.2620		-4.6004	-0.1473	-0.0499	0.4780
0.1909	-7.6496	-0.4521		0.5910		-6.5265	-0.4004		0.5390		-7.4888	-0.3654	-0.0832	0.9440
0.2879	-9.7808	-0.6340		0.7700		-8.6687	-0.5895		0.7030		-9.5824	-0.5533	-0.1089	1.1930
0.3861	-11.2247	-0.7699		0.9180		-9.9526	-0.7270	-0.1095			-11.0311	-0.6929	-0.1278	1.3240
0.4855		-0.8458		0.9940		-10.8296	-0.8105	-0.1216			-11.5313	-0.7818	-0.1356	1.3220
	-11.5478	-0.7412		0.8860		-10.5332	-0.6898	-0.1201		0.7010	-11.3980	-0.6689	-0.1356	1.1840
0.6876	-9.4760	-0.6137		0.7690		-8.5880	-0.5637		0.7220		-9.6627	-0.5207		0.9940
0.7905	-7.0899	-0.4755		0.5400		-6.4461	-0.4218	-0.0744			-7.4704	-0.3789	-0.0894	_
0.8946	-4.3851	-0.2587		0.2710		-3.2247	-0.2009	-0.0372	0.2260		-3.9486	-0.1668	-0.0470	0.4030
1.0000	0.0000	0.0000	0.0000	0.0000	1.0000	0.0000	0.0000	0.0000	0.0000	1.0000	0.0000	0.0000	0.0000	0.0000
							308.15K	I				I	ı	
0.0000	0.0000	0.0000		0.0000		0.0000	0.0000	0.0000	0.0000		0.0000	0.0000	0.0000	0.0000
0.0949	-5.0185	-0.2685		0.2420		-4.9962	-0.2689	-0.0508	0.2190		-5.6198	-0.2277	-0.0604	0.3140
0.1909	-7.9970	-0.5295	-0.0856	-		-8.0229	-0.4865		0.4760		-9.4916	-0.4900	-0.1048	0.7500
0.2879		-0.6901		0.6500		-9.8396	-0.6830		0.6270		-11.5439	-0.7005	-0.1301	0.9820
0.3861	-11.5639	-0.8131		0.8270		-11.3715	-0.8457		0.7260		-13.3871	-0.8485	-0.1539	1.1220
	-12.6706	-0.8914		0.8950		-12.6148	-0.9123		0.7810		-13.6246	-0.9118	-0.1586	1.1420
0.5860	-12.0016	-0.7929	-0.1364			-12.2780	-0.7926		0.7420		-13.7541	-0.8146	-0.1622	1.0060
0.6876	-9.8703	-0.6804		0.6520		-10.4970	-0.6792		0.6160		-12.2357	-0.6508	-0.1450	0.8490
0.7905	-7.7038	-0.5213	-0.0884			-8.1593	-0.5325	-0.0931	0.4340		-9.1008	-0.4859	-0.1076	0.5520
0.8946	-4.8068	-0.3226	-0.0554	1		-4.7174	-0.2616	-0.0540			-5.2100	-0.2290	-0.0613	0.2840
1.0000	0.0000	0.0000	0.0000	0.0000	1.0000	0.0000	0.0000	0.0000	0.0000	1.0000	0.0000	0.0000	0.0000	0.0000
							313.15K		I					10.0000
0.0000	0.0000	0.0000		0.0000		0.0000	0.0000	0.0000	0.0000		0.0000	0.0000	0.0000	0.0000
0.0949	-5.7767	-0.2966		0.1770		-6.0802	-0.3397	-0.0612	0.1850		-6.5898	-0.3076	-0.0698	0.2400
0.1909	-9.0076	-0.5597		0.3630		-9.2734	-0.5952		0.4070		-11.1844	-0.5982	-0.1219	0.6140
0.2879	-11.2967	-0.7271		0.5310		-11.2594	-0.7910		0.5630		-13.9161	-0.8483	-0.1551	0.8340
0.3861	-12.6280	-0.8390		0.7100		-13.1673	-0.9566	-0.1411	0.6480		-15.8768	-0.9949	-0.1805	0.9730
0.4855	-13.4475	-0.9199		0.7860		-14.2926	-1.0434		0.6860		-16.1829	-1.0459	-0.1864	1.0000
	-12.9357	-0.8409		0.7120		-14.2522	-0.9493		0.6630		-16.1554	-0.9469	-0.1883	0.8650
0.6876		-0.7297		0.5810		-12.5272	-0.8064		0.5410		-14.6675	-0.8100	-0.1719	0.7460
0.7905	-8.6832	-0.5714		0.3660		-10.0490	-0.6361	-0.1138			-10.9704	-0.5961	-0.1280	0.4740
0.8946	-6.1202	-0.3626		0.1570		-5.6227	-0.3225	-0.0636			-6.0565	-0.3347	-0.0700	0.2180
1.0000	0.0000	0.0000	0.0000	0.0000	1.0000	0.0000	0.0000	0.0000	0.0000	1.0000	0.0000	0.0000	0.0000	0.0000
							318.15K		I					10.0000
0.0000	0.0000	0.0000		0.0000		0.0000	0.0000	0.0000	0.0000		0.0000	0.0000	0.0000	0.0000
0.0949	-6.1921	-0.3423		0.1290		-7.3333	-0.4316	-0.0720	0.1690		-7.4716	-0.3653	-0.0777	0.1790
0.1909	-9.8957	-0.6038		0.2980		-10.6427	-0.7074		0.3580		-12.6020	-0.6777	-0.1350	0.5190
0.2879	-12.2489	-0.7710		0.4620		-12.7974	-0.9021	-0.1306	0.5080		-15.6177	-0.9711	-0.1711	0.7300
0.3861	-13.6647	-0.8821		0.6220		-14.6496	-1.0718		0.5850		-17.6717	-1.1186	-0.1975	0.8610
0.4855		-0.9476	-0.1574			-15.7172	-1.1710		0.6250		-18.1998	-1.1471	-0.2063	0.9150
0.5860		-0.8757		0.6550		-15.4819	-1.0861	-0.1678	0.6070		-18.0051	-1.0673	-0.2063	0.7830
0.6876		-0.7705		0.5120		-14.0245	-0.9510		0.4900		-16.3085	-0.9465	-0.1877	0.6580
0.7905	-9.5702	-0.6156		0.3030		-11.2197	-0.7350	-0.1241	0.3490		-12.2912	-0.6905	-0.1408	0.3990
0.8946	-6.7261	-0.3949		0.1150		-6.8441	-0.4104	-0.0759	0.1250	_	-7.0927	-0.3900	-0.0805	0.1710
1.0000	0.0000	0.0000	0.0000	0.0000	1.0000	0.0000	0.0000	0.0000	0.0000	1.0000	0.0000	0.0000	0.0000	0.0000

Figures 3(a), 3(b) and 3(c) show how excess free length varies across DMC compositions in the three systems studied. According to Ramamurthy and Sastry [19], negative  $L_{\rm f}^{\rm E}$  values suggest that sound waves must travel a greater distance. This could be due to dominating interactions between different molecules. The presence of ad and  $L_{\rm f}^{\rm E}$  minima at the same concentrations supports molecular connections.

Fig 4(a), 4(b) and 4(c) show negative viscosity deviations for all binary systems across the mole fraction range, with negative maximum values around 0.4 mole fractions. Viscosity varies based on the strength

of interactions between like and unlike molecules. The sign and magnitude of  $\Delta \eta$  vary with the structural features of liquid components due to differences in molecular size and shape, resulting from geometrical fitting.

Negative variations in viscosity may be caused by dispersion or dipolar forces between molecules due to their size and shape differences.

Physical interactions are often weak or strong, and the sign of  $\Delta\eta$  might be negative or positive. Positive values of  $\Delta\eta$  indicate strong intermolecular interactions, while negative values indicate lesser interactions between dissimilar molecules.

Specific chemical interactions between liquid mixture components, such as hydrogen bond formation and dipole-dipole interactions, cause the structure to become more compact and result in positive viscosity deviations. The sign and magnitude of  $\Delta\eta$  vary with the structural features of liquid components, resulting from geometrical fitting due to differences in molecular size and shape. In this scenario, all three systems have negative  $\Delta\eta$  values, indicating strong interactions such as interstitial accommodation. The results are in good agreement with those derived from data based on  $V^{\scriptscriptstyle E}$  and deviations in compressibility ( $\Delta\beta_{ad}$ )

Table 4 & 5 shows the actual values as well as the theoretical values computed using the Nomoto, Van Dael ideal mixing, impedance, Rao's specific velocity, and Junjie relationships for the analyzed systems at temperatures of 303.15, 308.15, 313.15, and 318.15K along with percentage of deviations. The validity of various theoretical formulae is evaluated by percentage deviation and chi square test for all the mixtures at all the temperatures, which are also shown in Table 4 & 5. It is assumed that all molecules are spherical, although this is not always the case. Nomoto's hypothesis assumes that the volume remains constant when mixed. As a result, no interactions between liquid mixture components were considered. The assumption for the establishment of an ideal mixing relation is that the specific heat ratios of ideal mixtures and volumes are equal. Again, no molecular interactions are taken into consideration.

Table 3: Experimental and theoretical velocities of DMC + MA, EA and BA systems using various theories

	DMC+Methyl Acetate										
Xı	UEXP	U <sub>nom</sub>	U <sub>IMP</sub>	Uvdv	$U_{\scriptscriptstyle JUN}$	Urao	U <sub>KUD</sub>				
303.15K											
0.0000	1106.0	1106.0	1106.0	1106.0	1106.0	1106.0	1106.0				
0.0949	1138.7	1111.8	1113.4	1111.9	1110.0	1128.7	1114.1				
0.1909	1165.2	1117.8	1120.8	1118.0	1114.4	1151.0	1121.8				
0.2879	1187.6	1124.1	1128.0	1124.3	1119.4	1169.8	1129.3				
0.3861	1207.0	1130.6	1135.1	1130.9	1124.9	1185.1	1136.6				
0.4855	1225.2	1137.3	1142.0	1137.6	1131.1	1196.4	1143.5				
0.5860	1230.0	1144.3	1148.9	1144.6	1138.0	1198.1	1150.3				
0.6876	1222.6	1151.6	1155.7	1151.9	1145.8	1197.3	1156.9				
0.7905	1212.8	1159.2	1162.3	1159.4	1154.5	1194.4	1163.2				
0.8946	1201.0	1167.1	1168.9	1167.2	1164.3	1186.5	1169.3				
1.0000	1175.3	1175.3	1175.3	1175.3	1175.3	1175.3	1175.3				
				.15K							
0.0000	1102.9	1102.9	1102.9	1102.9	1102.9	1102.9	1102.9				
0.0949	1136.5	1107.2	1108.4	1107.3	1105.6	1126.2	1108.8				
0.1909	1160.0	1111.6	1113.7	1111.9	1108.7	1148.0	1114.4				
0.2879	1182.0	1116.2	1119.0	1116.6	1112.2	1164.2	1119.9				
0.3861	1197.6	1120.9	1124.2	1121.4	1116.2	1177.2	1125.2				
0.4855	1214.0	1125.9	1129.3	1126.4	1120.7	1186.7	1130.3				
0.5860	1217.0	1131.0	1134.4	1131.5	1125.8	1186.8	1135.3				
0.6876	1207.3	1136.3	1139.3	1136.8	1131.6	1184.6	1140.1				
0.7905	1198.0	1141.9	1144.2	1142.2	1138.1	1178.8	1144.8				
0.8946	1183.0	1147.7	1149.0	1147.9	1145.4	1169.6	1149.3				
1.0000	1153.7	1153.7	1153.7	1153.7	1153.7	1153.7	1153.7				
				.15K							
0.0000	1083.5	1083.5	1083.5	1083.5	1083.5	1083.5	1083.5				
0.0949	1120.1	1087.8	1089.0	1088.0	1086.3	1107.5	1089.4				
0.1909	1144.5	1092.3	1094.5	1092.6	1089.5	1129.0	1095.2				
0.2879	1165.6	1097.0	1099.8	1097.3	1093.1	1145.2	1100.7				
0.3861	1181.8	1101.8	1105.1	1102.2	1097.2	1157.6	1106.1				
0.4855	1195.5	1106.8	1110.3	1107.3	1101.8	1167.1	1111.3				
0.5860	1200.1	1112.0	1115.4	1112.5	1106.9	1168.3	1116.3				
0.6876	1192.6	1117.4	1120.4	1117.8	1112.8	1166.4	1121.2				

0.7005	1102 5	1122.0	1125.3	1122 /	1119.3	1160.9	1126.0						
			1130.2				1130.5						
			1135.0				1135.0						
1.0000	1133.0	1133.0		.15K	1155.0	1133.0	1133.0						
0.0000	1062.9	1062.9		1062.9	1062.9	1062.9	1062.9						
1		1067.1		1067.3			1068.7						
		1071.5		1071.7			1074.3						
			1078.8				1079.7						
			1083.9										
			1089.0			1146.1							
			1093.9			1147.4							
			1098.8			1145.8							
0.7905			1103.6			1140.4	1104.2						
			1108.4					1C+Eth	vl Acote	ıto.			1
1.0000	1113.0	1113.0	1113.0	1113.0	1113.0	1113.0	1113.0	CIE				1	
					X <sub>1</sub>	$U_{EXP}$	U <sub>nom</sub>	U <sub>IMP</sub>	U <sub>vov</sub>	$U_{\text{JUN}}$	U <sub>RAO</sub>	U <sub>KUD</sub>	
								303.					
					0.0000	1117.3		1117.3		1117.3			
					0.1144	1147.0		1125.0	1123.4		1130.2		
T	fable 4	4 Perc	entag	e		1171.0				1124.1			Deviations and Interaction
	Para	meter	s (a)			1193.6				1128.3			
						1211.3				1133.1			
					0.5376	1227.0		1151.0	1147.0	1138.5	1180.0		
					0.6356	1234.0		1156.4 1161.6	1152.8				
					0.7307	1225.5 1215.0		1166.4		1151.1			
					0.8230 0.9128	1195.1		1171.0	1164.1 1169.7		1182.3 1178.6		
					1.0000			1175.3					
								308.					
					0.0000	1095.2	1095.2	1095.2	1095.2	1095.2	1095.2	1095.2	
					0.1144	1130.0	1101.0	1103.0	1101.3	1098.3	1111.2	1102.2	
					0.2252	1156.0	1106.7	1110.2	1107.3	1102.0	1125.6	1108.9	
					0.3326	1175.7	1112.5	1117.0	1113.3	1106.3	1139.4	1115.3	
					0.4367	1195.0	1118.3	1123.3	1119.2	1111.1	1152.1	1121.4	
					0.5376	1214.0	1124.2	1129.2	1125.1	1116.5	1161.2	1127.3	
					0.6356	1221.2	1130.0	1134.7	1130.9	1122.6	1163.0	1133.0	
					0.7307	1215.2	1135.9	1139.9	1136.7	1129.3	1164.6	1138.5	
					0.8230	1204.1	1141.8	1144.7	1142.4	1136.7	1164.6	1143.7	
						1184.0			1148.1				
					1.0000	1155./	1155./	1153.7 <b>313.</b>		1155./	1155./	1155./	
					0.0000	1080.7	1080.7	1080.7		1080.7	1080.7	1080.7	
						1120.0		1087.9		1083.5			
						1146.0		1094.7	1092.0		1113.6		
						1166.3		1100.9	1097.6	1090.8	1126.9	1099.3	
					0.4367	1188.0	1102.2	1106.8	1103.1	1095.2	1139.3	1105.0	
					0.5376	1205.5	1107.6	1112.2	1108.5	1100.2	1148.8	1110.5	
					0.6356	1215.0	1113.0	1117.4	1113.9	1105.9	1151.2	1115.8	
					0.7307	1210.0	1118.5	1122.2	1119.3	1112.1	1151.5	1120.9	
					0.8230	1198.2	1124.0	1126.7	1124.6	1119.0	1150.3	1125.8	
						1170.7				1126.7			
					1.0000	1135.0	1135.0	1135.0		1135.0	1135.0	1135.0	
					0.0000	1052.4	1052.4	318. 1052.4		1052.4	1052.4	1052.4	
					0.0000 0.1144	1052.4		1052.4	1052.4		1052.4		
						1122.0		1068.0	1056.7		1073.3		
						1143.4		1075.0	1071.1		1103.4		
						1164.7		1073.0		1069.0			
						1182.1		1087.6	1083.3		1127.0		
					0.6356	1191.0		1093.3	1089.3		1130.6		
						1190.0		1098.7	1095.3		1132.1		
					0.8230	1178.0		1103.7		1095.4			
DOI: 1	10.979	0/486	1-1706	50125				110%/5 <sub>W</sub>					7   Page
1		250	2,00					1113.0			_		, , , , , , , , , , , , , , , , , , , ,
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X.   UEXP   UMOM   UINIBOR ST   VIVI   UINO   URAD   UKUD   URAD   URA			I	OMC+M	ethyl Ace	etate		
0.0000	X <sub>1</sub>	%U <sub>N</sub> 9	%U <sub>imp</sub>   % <u></u>		<del>,                                    </del>			
0.0000		_		UIMB0	3. <b>₫\$Ĭ</b> Š	UJUN U	IRAO U	
0.1499								0.0000
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$\begin{array}{c} 0.58502 & -1255.4 & 6.78932 & 97.1491 & 70.36813 & 1.762.35241 & 164.7652 & 1.301.599 & 118.9579 \\ 0.68698 & -129076.0 & 6.51490.9 & 94.1171.8 & 47731.712.58971 & 165.42841 & 1.51.548 & 11.90.548 \\ 0.68698 & -128076.9 & 5.41771.9 & 5.7868 & 72.52.8421.72.17201 & 165.3841 & 15.1288 & 11.90.548 \\ 0.7868 & -128076.9 & 4.16182.8 & 4.011873.4 & 805$1.731.5191 & 168.8741 & 15.1286 & 11.90.942 \\ 0.7868 & -128238.6 & 2.61683.7 & 2.8141.74.3 & 95761.731.5191 & 168.8741 & 15.90.442 & 11.90.942 \\ 0.8862 & -128238.6 & 2.61683.7 & 2.8141.74.3 & 95761.731.8103 & 1176.3556 & 114.0388 & 11.95.88 \\ 0.9330 & 0.9910.4 & 0.0000 & 0.0000 & 300.81.548 & 11.75.3 &$								
$\begin{array}{c} 0.58698 & -19266 - 6.5440 , 96.941   71.8   4773   1772   5897   165.2784   155.1248   1190.548 \\ 0.68698 & -18205 - 5.4771 , 95.7861   72.52842   172.7020   165.2784   155.1248   1190.548 \\ 0.7848 & -12205 - 4.16182 , 24.4011   73.3   8055   173.0   191.66.28   47.1150   47.240 \\ 0.8824 & -12825 - 6.2767 , 37.8117 , 43.0576   173.8   2103   170.3556   1140.388   1190.588 \\ 0.9990 & 0.9990 & 0.9990 & 0.9990 & 0.9990 & 1.9990   174.9000   17$								
$\begin{array}{c} 0.686 - \frac{5}{8}105 - \frac{5}{2}4771 - \frac{5}{2}^{8}781 + \frac{5}{2} - \frac{5}{2}841 + \frac{5}{2} + \frac{20}{2} - 1166.68^{2} - \frac{11}{2}136.66^{2} - 1171.26^{2} \\ 0.7848 - \frac{14}{2}268 - \frac{4}{16}1872.8^{4}401173.3^{4}8051173.0^{5}191166.88^{2}41139.042^{2} + 1172.972.08824^{2} - \frac{12828}{2}6.267693.7^{2}814174.1^{3}0576173.8^{2}1031170.356611.40388 + 1179.588^{2}0.49336 - 0.90004.0.90004 - 0.90000 - 0.900$								
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$\begin{array}{c} 0.8821 & -2328.6 - 21783. 7.2814174. \stackrel{?}{1}.30576173. \stackrel{?}{8}1031170. \stackrel{?}{6}356116. \stackrel{?}{4}3881173. \stackrel{?}{5}861. \stackrel{?}{6}43881173. \stackrel{?}{5}81173. \stackrel{?}{5}811174. \stackrel{?}{5}81173. \stackrel{?}{5}811174. \stackrel{?}{5}811174. \stackrel{?}{5}811174. \stackrel{?}{5}811174. \stackrel{?}{5}811174. \stackrel{?}{5}811174. \stackrel{?}{5}811174. \stackrel{?}{5}811175. \stackrel{?}{5}811175. \stackrel{?}{5}811175. \stackrel{?}{5}81175. \stackrel{7}{5}81175. \stackrel{?}{5}81175. \stackrel{?}{5}$								
$\begin{array}{c} 0.9000 & 0.0000 & 0.0000 & 1.74 & 0.0001 & 74 & 0.000 & 11.72 & 0.000 & 11.72 & 0.000 & 11.74 & 0.000 & 11.74 & 0.000 & 1.0000 & 1.0000 & 0.$								
00000								
$\begin{array}{c} 00000 & 17389 - 24754 - 34.561 + 94.7771 + 94.949 - 1149.4708 + 149.334 + 149.334 \\ 0.1909 & 41732 - 318749 + 34.1915 - 1.4915 - 1.0332 + 134.9290 \\ 0.1479 & 11920 - 31449 + 94.1915 - 1.1915 - 1.0332 + 134.9290 \\ 0.2889 & 52688 - 53275 - 55.53675 0.5 5.03675 0.5 90.2115 0.5072 + 145.2539 + 1134.107 + 1150.24 \\ 0.2809 & 1225.5 - 5.3175 0.5 5.53675 0.5 90.2115 0.5072 + 145.2539 + 1134.107 + 1150.24 \\ 0.3401 & -64206 - 6.1265 1.6 -3641 5 1.5 -9.7954 1.5 1.7029 + 145.8456 + 1131.3406 + 1150.29 \\ 0.94865 & -72652 - 7.6651 - 6.7891 - 8.7026 5 -7.4925 1.5 1.2 -24815 1.46.932 + 1136.5 + 1151.3 \\ 0.5860 & -7.0661 - 6.7891 - 8.7026 5 -7.4925 1.5 1.2 -24815 1.46.7137 + 1416.9 + 1151.8 \\ 0.7610 & -12745 - 5.5342 - 5.4415 2.2 - 6.2730 1.5 1.2 -8788 + 147.35 + 1142.17 + 10.1617 \\ 0.7896 & -72875 - 5.5352 - 5.4415 2.2 - 5.003 1.5 1.2 -5.007 1.48 + 140.4 + 1151.8 \\ 0.7610 & -12745 - 5.5332 - 2.9691 1.5 3.2 - 1152.3 + 174.3 + 1142.17 + 10.22.2 \\ 0.7848 & -12834 - 4.4912 - 4.6546 - 15.25 + 0.033 1.5 1.2 -6007 1.48 + 32.11 + 14.990 1.5 2.6 \\ 0.8824 & -23861 - 2.8753 . 0.9691 1.5 3.2 -1785 1.153.1 + 150.000 0.0$	1,0000	1175.2	1174.5	1174.7	1174.6 8.15 <b>K</b> 2	1172.8 1	175.2	174.5
$\begin{array}{c} 00000 & -15809 - 247549 \cdot 24^{-5}61^3 + 94^{-24}71^7   149^9 \cdot 49108^4 \cdot 1149^4 \cdot 4149^3 \cdot 1149^3 \cdot 4149^3 \cdot 4149$	0.0000	0.0000 (	0.0000 0.	0000 308	000 0.000 0.15K	0.0000	1.0000	0.0000
$\begin{array}{c} 0.2899 & -5.5688 - 5.32716 \\ 0.3861 & -6.2466 \\ 0.61265 & -1765 \\ 0.3861 & -6.2466 \\ 0.61265 & -1765 \\ 0.3861 & -1965 \\ 0.64011 & -12466 \\ 0.61265 & -1765 \\ 0.63611 \\ 0.5165 & -1765 \\ 0.7562 & -1765 \\ 0.$	0.0049	<del>-2.5809 -</del> 1149.4	<del>2.4752 -2.</del> 1149.4	5675 1149.4	171 <u>-0.90</u> 4 1149.4	<del>15 -2.4408</del> 1149.4 1	149.4 1	0.0534 149.4
$\begin{array}{c} 0.3861 & -6.4016 - 6.1262 & 0.63611 & 1.6.7954 & 1.51.7029 & 148.856 & 1133.1406 & 19.1406 \\ 0.4865 & 7.7589.2 - 6.9731 & 7.2113 & 1.76831 & 15.75251 & 1145.8924 & 1136.517 & 1151.37 \\ 0.5860 & 7.0661 & 6.7891 & 7.0266 & 5.74925 & 15.12.31 & 146.47 & 1140.45 & 1151.87 \\ 0.6876 & -1877.6 & 5.63152 & 5.841 & 5.26.2730 & 15.12.3788 & 145.5554 & 1142.179 & 19.1269 \\ 0.6876 & -1877.6 & 5.63152 & 5.841 & 5.26.2730 & 15.12.3788 & 145.5554 & 1143.99 & 1152.20 \\ 0.77905 & -468347 & -4.4912 & 4.6546 & 152.5 & 5.0033 & 152.7 & 148.52 & 1143.99 & 1152.80 \\ 0.8824 & -23821 & -2.8763 & 2.9691 & 153.3 & 1785 & 153.1365 & 152.08 & 1144.92 & 1153.00 \\ 0.8824 & -23821 & -2.8763 & 2.9691 & 153.3 & 1785 & 153.1365 & 152.08 & 1144.92 & 1153.00 \\ 0.99336 & -1197.8 & -1153.4 & -1153.3 & 1153.4 & 1151.8 & 1149.5 & 1153.3 & 1.0000 & 0.00$								
$\begin{array}{c} 0.4855 & 7.7592 - 6.9731 & 7.2133 & 7.86831 & 51.2513 & 1145.8924 & 1136.517 & 10.1617 \\ 0.5868 & 7.0661 & 6.7891 & 7.0266 & 5.7.4925 & 5.2.4815 & 16.7137 & 1140.49 & 1151.8 \\ 0.6876 & 1270.5 & 1151.8 & 7.0266 & 5.7.4925 & 5.2.4815 & 146.47 & 1140.49 & 1151.8 \\ 0.6876 & 1270.5 & 6.152.2 & 5.841 & 52.6.2730 & 15.1.8788 & 145.5554 & 1142.179 & 10.2279 \\ 0.7848 & 1261.7 & 1152.6 & 6152.5 & 60033 & 152.7 & 1145.5954 & 1142.179 & 10.2279 \\ 0.7848 & 1261.7 & 1152.6 & 1152.5 & 60033 & 152.7 & 1143.59 & 1152.8 \\ 0.8824 & 12821.5 & 1753.0 & 12.9691 & 153.2 & 1785.1 & 153.1 & 153.0 & 1144.92 & 1153.0 \\ 0.8824 & 12821.5 & 1753.0 & 12.9691 & 153.2 & 1785.1 & 153.1 & 153.0 & 1144.92 & 1153.0 \\ 0.8824 & 12821.5 & 1753.0 & 12.9691 & 153.2 & 1785.1 & 153.1 & 153.0 & 1144.92 & 1153.0 \\ 0.8824 & 12821.5 & 1753.0 & 12.9691 & 153.2 & 1785.1 & 153.1 & 153.0 & 1144.92 & 1153.0 \\ 0.8824 & 12821.5 & 1753.0 & 0.0000 & 0.00000 & 0.0000$								
$\begin{array}{c} 0.5860 & -7.0661 & 6.7891 & 7.0266 & 2.74925 & 1.24815 & 6.7137 & 1141.569 & 1151.8 & 1152.8 & 1151.8 & $								
$\begin{array}{c} 0.686^{2} & 5.8774.6 & 5.6394 & 5.841352.6 & 2730152.3 & 81142.55654 \\ 0.79848 & 1261.7 & 4.9142.6 & 6.54652.5 & 0.033152.6 & 0.0671148.5 & 1142.179 & 10.122.6 \\ 0.89246 & -2.9861.5 & 2.8753.0^{2}.96915.3 & 1.78513.1 & 152.1 & 152.0 & 1147.9 & 1152.0 \\ 0.89246 & -2.9861.5 & 2.8753.0^{2}.96915.3 & 1.78513.1 & 152.0 & 1147.9 & 1153.0 & 1.0000 & 0.$	0.00							
$\begin{array}{c} 0.7985 & 4.8834 - 4.4914 - 2.4.6.6.516.52.50031 15.2.76017 + 4.4427 \\ 0.8946 & -2.9861 - 2.8753 .0^{2.969} 15.3.7 1851 .133.1^{2.6067} 1148.2^{4.27} 1143.900 & 19.000 \\ 0.8946 & -2.9861 - 2.8753 .0^{2.969} 15.3.2^{2.1785} 1153.1^{1365} 1150.0^{8.4177} 1147.7^{2.119.000} 1.9000 \\ 1.9000 & 0.9000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.9336 & 1197.8 & 1153.4 & 1153.3 & 1158.4 & 1151.8 & 1149.3 & 1153.3 \\ 1.0000 & 1.153.7 & 1153.0 & 1130.1 & 130.1 $								
$\begin{array}{c} 0.8861 & 2.2861 & 2.2875 & 2.7861 & 3.2.1785 & 5.1.365 & 15.2.8483 & 1.4621 & 10.962 \\ 1.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 1.0000 & 1.0000 \\ 1.0000 & 1.0000 & 0.0000 & 0.0000 & 0.0000 & 1.0000 & 1.0000 & 1.0000 \\ 0.9330 & 1197.8 & 1153.7 & 1153.7 & 1153.7 & 1153.7 & 1153.7 & 1153.7 \\ 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.0000 & 1130.1 & 0.2879 & 5.8866 & 5.6421 & 5.8869 & -6.2172 & -1.7485 & 5.5638 & 1.1283 & 0.1283 & 0.2809 & 1215.0 & 1131.3 & 1131.7 & 1131.4 & 1127.3 & 1118.2 & 1131.2 & 0.3861 & -6.8661 & -6.4867 & -6.7305 & -7.1552 & -2.0423 & -6.4006 & 1.1495 & 0.1495 & 0.4911 & 1241.0 & 1131.9 & 1132.3 & 1132.0 & 1126.9 & 1119.5 & 1131.8 & 0.4855 & -7.4147 & -7.1267 & -7.3805 & -7.8383 & -2.3718 & -7.0411 & 1.1657 & 0.1657 & 0.5102 & 1262.0 & 1132.4 & 1132.8 & 1132.5 & 1127.0 & 1122.4 & 1132.8 & 0.5860 & -7.3399 & -7.0598 & -7.3034 & -7.7625 & -2.6522 & -6.6991 & 1.1638 & 0.1638 & 0.6876 & -6.3039 & -6.0544 & -6.2706 & -6.6952 & -2.1980 & 5.9850 & 1.1383 & 0.1383 & 0.7905 & 5.1100 & -4.9161 & 5.0835 & 5.4264 & 1.9098 & 4.8641 & 1.1100 & 0.1100 & 0.7848 & 1258.9 & 1133.8 & 1133.8 & 1134.4 & 1133.4 & 1123.5 & 1128.8 & 1133.8 & 1134.2 & 1133.4 & 1123.5 & 1128.8 & 1133.8 & 1134.2 & 1133.4 & 1123.5 & 1128.8 & 1133.5 & 1133.0 & 1134.6 & 1133.1 & 1134.1 & 1133.1 & $								
$\begin{array}{c} 1,0000 & 0,0000 & 0,0000 & 0,0000 & 0,0000 & 0,0000 & 0,0000 & 1,0000 & 0,0000 \\ 0.9336 & 1197.8 & 1153.4 & 1153.3 & 1153.7 & 1153.7 & 1153.7 & 1153.7 \\ 0.0000 & 0.0000 & 0.0000 & 0.00000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.0000 & 1.153.7 & 1153.7 & 1153.7 & 1153.7 & 1153.7 & 1153.7 \\ 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.0000 & 1130.1 & 113$								
1.0000	0.8621							
$\begin{array}{c} 0.0999 \\ 0.0000 \\ 0.0000 \\ 1130.1 \\ 1130.$	0.9336	1197.8	1153.4	1153. <b>3</b> 1	3.15K 4			
$\begin{array}{c} 0.0999 \\ 0.0000 \\ 0.0000 \\ 1130.1 \\ 1130.$	0.0000	0.0000 (	0.0000 0.	0000 313	000 0.000	0.0000	1.0000	0.0000
$\begin{array}{c} 0.1909 - 4.5599 - 4.3721 - 4.5376 - 4.8054 - 1.3550 - 4.3097 - 1.0973 - 0.0973 \\ 0.1479 - 11770 - 1130.7 - 1131.0 - 1130.8 - 1128.3 - 1121.2 - 1130.7 \\ 0.2809 - 1215.0 - 1131.3 - 1131.7 - 1131.4 - 1127.3 - 1118.2 - 1131.2 \\ 0.3861 - 6.7651 - 6.4867 - 6.7305 - 7.1552 - 2.0423 - 6.4006 - 1.1495 - 0.1495 \\ 0.4011 - 1241.0 - 1131.9 - 1132.3 - 1132.0 - 1126.9 - 1119.5 - 1131.8 \\ 0.4011 - 1241.0 - 1131.9 - 1132.3 - 1132.0 - 1126.9 - 1119.5 - 1131.8 \\ 0.4855 - 7.4174 - 7.1276 - 7.3805 - 7.8583 - 2.3718 - 7.0411 - 1.1657 - 0.1657 \\ 0.5102 - 1262.0 - 1132.4 - 1132.8 - 1132.5 - 1127.0 - 1122.4 - 1132.3 \\ 0.5860 - 7.3399 - 7.0598 - 7.3034 - 7.7625 - 2.6532 - 6.9791 - 1.1638 - 0.1638 \\ 0.6876 - 6.3039 - 6.0544 - 6.2706 - 6.6952 - 2.1980 - 5.9850 - 1.1338 - 0.133.8 \\ 0.7010 - 1271.0 - 1133.4 - 1133.7 - 1133.4 - 1128.5 - 1128.0 - 1133.3 \\ 0.7905 - 5.1100 - 4.9161 - 5.0835 - 5.4264 - 1.9098 - 4.8641 - 1.100 - 0.100 \\ 0.8621 - 1225.4 - 1134.2 - 1134.4 - 1134.3 - 1133.7 - 1128.1 - 1131.3 - 1133.7 \\ 0.8946 - 3.7275 - 3.6161 - 3.7119 - 3.9171 - 1.7760 - 3.5872 - 1.0786 \\ 0.9336 - 1183.0 - 1134.4 - 1134.4 - 1134.6 - 1134.1 - 1135.0 - 1135.0 \\ 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 \\ 0.9336 - 1183.0 - 1135.0 - 1135.0 - 1135.0 - 1135.0 - 1135.0 - 1135.0 \\ 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 \\ 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 \\ 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 - 0.0000 \\ 0.0000 - 1135.0 $	0.0949	-2.8/0/	2.7090 -2.	<del>8044 -3.0</del>	1130.1	1130.1 1	1.0398	0.0394
$\begin{array}{c} 0.2899 & 5.8866 & 5.6421 & 5.8569 & 6.2172 & 1.7485 & 5.5638 & 1.1283 & 0.1283 \\ 0.2809 & 1215.0 & 1313.1 & 1131.7 & 1131.4 & 1127.3 & 1118.2 & 1131.2 \\ 0.3861 & 6.7651 & 6.4867 & 6.7305 & 7.1552 & 2.0423 & 6.4006 & 1.1495 & 0.1495 \\ 0.4011 & 1241.0 & 1131.9 & 1132.3 & 1132.0 & 1126.9 & 1119.5 & 1131.8 \\ 0.4855 & 7.4174 & 7.1276 & 7.3805 & 7.8383 & 2.3718 & 7.0411 & 1.1657 & 0.1657 \\ 0.5102 & 1262.0 & 1132.4 & 1132.8 & 1132.5 & 1127.0 & 1122.4 & 1132.3 \\ 0.5860 & 7.3399 & 7.0598 & 7.3304 & 7.7625 & 2.6632 & 6.9791 & 1.1638 & 0.1638 \\ 0.6876 & 6.3039 & 6.0544 & 6.2706 & 6.6952 & 2.1980 & 5.5980 & 1.1383 & 0.1383 \\ 0.7010 & 12710 & 1133.4 & 1133.7 & 1133.4 & 1128.5 & 1128.0 & 1133.3 \\ 0.7010 & 12710 & 1133.4 & 1133.7 & 1133.4 & 1128.5 & 1128.0 & 1133.3 \\ 0.7905 & 5.1100 & 4.9161 & 5.0835 & 5.4264 & 1.9098 & 4.8641 & 1.110 & 0.1100 \\ 0.7848 & 1258.9 & 1133.8 & 1134.1 & 1133.9 & 1129.8 & 1131.0 & 1133.7 \\ 0.8946 & -3.7275 & -3.6161 & -3.7119 & -3.9171 & -1.7760 & 3.5872 & 1.0786 \\ 0.0786 & 0.9336 & 1138.0 & 1135.0 & 1135.3 & 1134.2 \\ 1.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.9336 & 1138.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 \\ 0.0000 & 1.35.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 \\ 0.92869 & -92080 & -84070 & -84770 & 74.7627 & 10.90371 & 110.42961 & 116.4277 & 11.109408 & 11.00948 \\ 0.92869 & -92080 & -84077 & -76771 & 74.7627 & 10.90371 & 110.42961 & 116.4277 & 11.101.4252 & 11.11.429 \\ 0.92869 & -92080 & -84077 & -74771 & -74797 & 1112.4292 & 110.4348 & 110.42452 & 11.11.439 \\ 0.94869 & -725880 & 7.26741 & 9.5071 & 11.25.9974 & 11.25.2901 & 10.4968 & 10.61889 & 11.11.5248 \\ 0.96869 & -725880 & 7.26741 & 9.5074 & 12.59991 & 11.25.29070 & 11.06.4868 & 10.61889 & 11.11.4453 \\ 0.96869 & -725880 & 7.26741 & 9.5074 & 12.59991 & 11.25.29070 & 11.06.4868 & 10.61889 & 11.11.445 \\ 0.96869 & -725880 & 7.26741 & 9.50741 & 12.59991 & 11.25.29070 & 11.06.4868 & 10.61889 & 11.19.445 \\ 0.96869 & -725880 & 7.26741 & 9.50741 & 12.59992 & 11.125.29070$		-4.5599	4.3721 -4.	5376 -4.8	054 -1.355	50 -4.3097	1.0973	0.0973
$\begin{array}{c} 0.3861 & -6.7651 - 6.4867 & -6.7305 & -7.1552 & -2.0423 & -6.4006 & 1.1495 & 0.1495 \\ 0.4011 & 1241.0 & 113.9 & 1132.3 & 1132.0 & 1126.9 & 1119.5 & 1131.8 \\ 0.4855 & -7.4174 - 7.1276 & -7.3805 & -7.8383 & -2.3718 & -7.0411 & 1.1657 & 0.1657 \\ 0.5102 & 1262.0 & 1132.4 & 1132.8 & 1132.5 & 1127.0 & 1122.4 & 1132.3 \\ 0.5860 & -7.3399 & -7.0598 & -7.3034 & -7.7625 & -2.6532 & -6.9791 & 1.1638 & 0.1638 \\ 0.6876 & -6.3039 & -6.0544 & -6.2706 & -6.6952 & -2.1980 & 5.9850 & 1.1383 & 0.1383 \\ 0.7010 & 1271.0 & 1133.4 & 1133.7 & 1133.4 & 1128.5 & 1128.0 & 1133.3 \\ 0.79015 & -1100 & -4.9161 & -5.0835 & -5.4264 & -1.9098 & 4.8641 & 1.1100 & 0.1100 \\ 0.7848 & 1258.9 & 1133.8 & 1134.1 & 1133.9 & 1129.8 & 1131.0 & 1133.7 \\ 0.8946 & -3.7275 & -3.6161 & -3.7119 & -3.9171 & -1.760 & -3.8872 & 10.786 & 0.0786 \\ 0.8621 & 1225.4 & 1134.2 & 1134.4 & 1134.3 & 1131.3 & 1133.1 & 1134.2 \\ 1.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 1.0000 \\ 0.9336 & 1183 & 0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 \\ 0.0000 & 1.35.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 \\ 0.0000 & \frac{7}{4}8^{1}6^{1}6^{1}6^{1}6^{1}6^{1}6^{1}6^{1}6$		1215.0	5.6421 -5. 1131.3	8569 -6.2 1131.7	172 -1.748 1131.4	1127.3 1	1.1283 118.2 1	0.1283 131.2
$\begin{array}{c} 0.5860 & 7.3399 & 7.0598 & 7.3034 & 7.7625 & 2.6532 & 6.9791 & 1.1638 & 0.1638 \\ 0.6098 & 1268.0 & 1132.9 & 1133.3 & 1133.0 & 1127.6 & 1126.1 & 1132.8 \\ 0.6876 & -6.3039 & -6.0544 & -6.2706 & -6.6952 & 2.1980 & 5.9850 & 1.1383 & 0.1383 \\ 0.7010 & 1271.0 & 1133.4 & 1133.7 & 1133.4 & 1128.5 & 1133.3 & 1133.3 \\ 0.7905 & -5.1100 & -4.9161 & 5.0835 & -5.4264 & 1.9998 & 4.8641 & 1.1100 & 0.1100 \\ 0.7848 & 1258.9 & 1133.8 & 1134.1 & 1133.9 & 1129.8 & 1131.0 & 1133.7 \\ 0.8946 & -3.2757 & -3.6161 & -3.7119 & -3.9171 & -1.7760 & -3.5872 & 1.0786 & 0.0786 \\ 0.8621 & 1225.4 & 1134.2 & 1134.4 & 1134.3 & 1133.3 & 1133.1 & 1134.2 \\ 1.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.9336 & 1183.0 & 1134.6 & 1134.7 & 1134.6 & 1133.1 & 1134.9 & 1134.6 \\ 1.0000 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 \\ 0.0000 & 0.0000 & 0.0000 & 0.0000 & 398995 K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 747674 & 747670 & 74.7671 & 75.9671 & 10.4961 & 1176.7791 & 116.9498 & 1176.9498 \\ 0.94891 & -4.78676 & 4.59770 & 74.7671 & 75.971 & 116.7931 & 16.7760 & 1106.733 & 1174.532 \\ 0.94891 & -6.92870 & -6.74771 & 5.961 & 11.76.3974 & 117.7693 & 106.3761 & 106.7351 & 117.769 \\ 0.94891 & -6.92870 & -6.74771 & 5.961 & 11.76.3974 & 117.7681 & 16.6354 & 106.75226 & 1174.754 \\ 0.94892 & -7.26771 & 5.9674 & 1.26.761 & 11.76.3974 & 117.7681 & 106.7460 & 106.7452 & 1174.754 \\ 0.94892 & -7.26770 & -7.7671 & 5.961 & 11.76.3974 & 117.76840 & 106.73468 & 106.75226 & 1174.7540 \\ 0.94896 & -7.26870 & -7.26771 & 5.9674 & 1172.79974 & 1172.7992 & 1107.7688 & 106.1689 & 1174.7544 \\ 0.96898 & -7.26870 & -2.6771 & 5.9674 & 1.27.79974 & 1172.7292 & 107.7688 & 108.1689 & 1174.7849 \\ 0.96898 & -7.26870 & -2.6771 & 2.5971 & 2.59626 & 11.2220 & 1176.7688 & 108.1689 & 1174.7849 \\ 0.96898 & -7.26870 & -2.67871 & 2.5971 & 2.59626 & 11.2220 & 1176.7868 & 108.1689 & 1174.7849 \\ 0.96898 & -7.26870 & -2.67871 & 2.5971 & 2.59626 & 11.2220 & 1176.7688 & 108.1689 & 1174.7849 \\ 0.96898 & -7.26870 & -2.67871 & 2.5971 & 2.59626 & 11.$	0.3861 0.4011	1241.0	1131.9	.7305 -7.1 1132.3	552 -2.042 1132.0	1126.9 1		
$\begin{array}{c} 0.6098 & 1268.0 & 1132.9 & 1133.3 & 1133.0 & 1127.6 & 1126.1 & 1132.8 \\ 0.6876 & 5.0399 & 6.0544 & 6.2706 & 6.6952 & -2.1980 & 5.9850 & 1.133.3 & 0.1383 \\ 0.7010 & 1271.0 & 1133.4 & 1133.7 & 1133.4 & 1128.5 & 1128.0 & 1133.3 \\ 0.7905 & 5.1100 & 4.9161 & 5.0835 & -5.4264 & 1.9098 & 4.8641 & 1.100 & 0.1100 \\ 0.8946 & -3.7275 & -3.6161 & -3.7119 & -3.9171 & -1.7760 & -3.5872 & 1.0786 & 0.0786 \\ 0.8621 & 1225.4 & 1134.2 & 1134.4 & 1134.3 & 1131.3 & 1133.1 \\ 1.0000 & 0.0000 & 0.0000 & 0.00000 & 0.0000 & 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.9336 & 1183.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 \\ 1.0000 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 \\ 0.0000 & 0.0000 & 0.0000 & 0.0000 & 39.8995 K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 7.976 & 7.4767 & 7.4767 & 10.5967 & 110.4961 & 116.4779 & 116.4968 & 116.9928 \\ 0.92869 & -928680 & -84770 & 7.4767 & 10.5967 & 110.42961 & 116.4779 & 116.4968 & 116.4969 \\ 0.94861 & -92870 & 6.7477 & 1.5696 & 111.5438 & 1106.5354 & 106.1333 & 1171.552 \\ 0.95862 & -728870 & 6.7477 & 3.5876 & 111.54397 & 117.4488 & 1166.5354 & 106.1333 & 1171.552 \\ 0.95869 & -728860 & 7.26771 & 5.0576 & 111.5429 & 117.4680 & 116.1688 & 116.1689 & 116.1689 \\ 0.96869 & -728860 & 7.26771 & 5.0576 & 112.54961 & 117.54292 & 116.1688 & 116.1689 & 116.1689 \\ 0.96869 & -728860 & 7.26771 & 5.0576 & 112.54962 & 116.24961 & 116.1688 & 116.1688 & 116.1689 & 116.1689 \\ 0.96869 & -728860 & 7.26771 & 5.0576 & 112.54962 & 116.24961 & 116.1684 & 116.1688 & 116.$	0.5102			3805 -7.8 1132.8	383 -2.371 1132.5		122.4 1	132.3
$\begin{array}{c} 0.7010  1271.0  1133.4  1133.7  1133.4  1128.5  1128.0  1133.3  0.7905  5.1100  4.9161  5.0835  5.4264  1.9098  4.8641  1.1100  0.1100  0.7848  1258.9  1133.8  1134.1  1133.9  1129.8  1131.0  1133.7  0.8946  3.7275  3.6161  3.7119  -3.9171  1.7760  3.5872  1.0786  0.0786  0.08621  12.25.4  1134.2  1134.4  1134.3  1131.3  1133.3  1133.2  1134.2  1134.4  1134.3  1131.3  1133.3  1133.2  1134.2  1134.4  1134.4  1134.6  1133  1133.0  1135.0  1135.0  1.0000  0.00$		-7.3399 - 1268.0	7.0598 -7. 1132.9	3034 -7.7 1133.3	1133.0	1127.6 1	126.1 1	132.8
$\begin{array}{c} 0.7848 & 1258.9 & 1133.8 & 1134.1 & 1133.9 & 1129.8 & 1131.0 & 1133.7 \\ 0.8946 & 3.7275 & 3.6161 & 3.7119 & 3.9171 & 1.7760 & 3.8872 & 1.0786 & 0.0786 \\ 0.8621 & 1225.4 & 1134.2 & 1134.4 & 1134.3 & 1131.3 & 1133.1 & 1134.2 \\ 1.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.9336 & 1183 & 0 & 1134.6 & 1134.7 & 1134.6 & 1133.1 & 1134.9 & 1134.6 \\ 1.0000 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 \\ 0.0000 & 0.0000 & 0.0000 & 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.0000 & 398.98K 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.0000 & 1.35.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 & 1135.0 \\ 0.92870 & -4780.4 -47$				1133.7	1133.4	1128.5 1	128.0 1	133.3
$\begin{array}{c} 1.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.9336 & 1.183 & 0 & 1135 & 0 & 1135 & 0 & 1135 & 0 & 1135 & 0 & 1135 & 0 \\ 1.0000 & 1.135 & 0 & 1135 & 0 & 1135 & 0 & 1135 & 0 & 1135 & 0 & 1135 & 0 \\ 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 & 1.0000 & 0.0000 \\ 0.0000 & 74 & 74 & 74 & 74 & 74 & 74 & 74 $	0.7848	1258.9	1133.8	1134.1	1133.9	1129.8 1	131.0 1	133.7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.8621	1225.4	1134.2	1134.4	1134.3	1131.3 1	133.1 1	134.2
$\begin{array}{llllllllllllllllllllllllllllllllllll$	0.9336	_1183.0	1134.6			1133.1 1	134.9 1	134.6
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0.4499 -4.1867:0-4.59770.74.767910-50379110.42311108547911021825 1190.925 0.2868 -9.2868:0-5.85961.66.065\$111.5.43571111.79931105.776011001733 11941833 0.48691 -9.2287:0-6.74771.56.961111.76.39741117.41881106535411021452 11941552 0.54665 -7.2487:07.39891.87.6516111.812291117.64601108346811051926 11941876 0.66898 -7.2588:07.26941.97.507112:7.97941117.972221108146811081689 11941889 0.74676 -9.259412-6.30982.16.52\$912:5.962\$1122206711052440111041845 1192445	0º0 <del>000</del> 8	-494634-	2.81390.42				11004081	1 969608
0!4\$PF1 - 4.22\$7.0^6.7\P7-1.56.96\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\								
0!\$ff65 -74248707.3P8P1.67.651611:8-122P1117:6 <sup>3</sup> 4601106:34681105:1326111P4!.876 0!6868 -74256807.26Pf1.97.507112:7.979f1117:9 <sup>7292</sup> 1106:15681108!68911P4!689 0!36876 -942637!2-6.3PP82.1 <sup>6.52</sup> 8712:8-96261122:2 <sup>067</sup> 1109:3440111b!.94511P2:145	0.2879	-9:20080-	5.85P\$1.06	06 <b>55</b> 11 <del>-</del> 2.4	<sup>35</sup> 711 <b>1</b> <sup>1</sup> .7 <sup>99</sup>	93 <sub>110</sub> 57.77 <sup>60</sup> 1	10013331	1 P1 <sup>1</sup> .8 <sup>33</sup>
0!:6898 -7.25860-7.26941.97.507112:7.97941117:9 <sup>292</sup> 1106.1 <sup>968</sup> 1108 <sup>1</sup> 689 11141 <sup>6</sup> 89 0!:7876 -4.58 <u>9</u> 1.2-6.30982.1 <sup>6.52</sup> 8912:5.9626112 <sup>2</sup> 3 <sup>2</sup> 0671109 <sup>2</sup> 3 <sup>440</sup> 1111 <sup>6</sup> 15 <sup>45</sup> 1112.4 <sup>45</sup>	09.4861	-9:2287.0-	6.711771. <b>3</b> 6.	<sup>96</sup> ††11 <del>.</del> 7.3	<sup>97</sup> 4111 <sup>2</sup> .4 <sup>18</sup>	<sup>38</sup> 1106:5 <sup>354</sup> 1	10214521	1 911.352
0!#876 -9. <del>2\$3</del> 1.2-6.30P\$2.16.52\$912:\$. <sup>962</sup> \$112 <del>:</del> 2 <sup>967</sup> 110 <del>9</del> .2 <sup>440</sup> 1116!\$ <sup>45</sup> 11P2!4 <sup>45</sup>	09.54865	-7.2487.0-	7.39891.6 <sup>7</sup>	<sup>65</sup> 1611 <del>.</del> 8.1	<sup>220</sup> 111 <sup>2</sup> .6 <sup>40</sup>	<sup>50</sup> 110 <sup>7</sup> 6. <sup>3</sup> 4 <sup>168</sup> 1	1051.726 1	1 P1 <sup>1</sup> .726
	0.6898	-7. <b>53</b> 680-	7.26341.97	<sup>50</sup> 7112:7.9	79 <b>4</b> 11 <b>1</b> 2 <i>9</i> 29	<sup>92</sup> 110 <sup>7</sup> 6. <sup>1</sup> 7 <sup>868</sup> 1	10816891	1 P1 <sup>1</sup> .889
007848 -5.32434-5.19832 25.365512-5.718411224356110854901114146611102566	09:7876	-9.5571.2-	6.30982.16	<sup>52</sup> ∮912 <del>.</del> 9.9	626112 <sup>2</sup> .2 <sup>300</sup>	<sup>57</sup> 110 <sup>67:25440</sup> 1	11101.545	1 P2!.44 <sup>\$</sup>
	0.7848	-124334-	<sup>5.1</sup> 9832.4 <sup>5</sup>	36§§12.5.7	<sup>184</sup> 112.4 <sup>35</sup>	<sup>56</sup> 11 <b>0</b> 8.5 <sup>490</sup> 1	11 <sup>1</sup> 4 <sup>1</sup> .0 <sup>66</sup> 1	1 921.366
0 <sup>0</sup> 88 <del>2</del> 16 -326847-3.89142.6 <sup>3.90</sup> 9412 <del>.4</del> .1119112 <sup>1</sup> .8 <sup>505</sup> 1109.7 <sup>873</sup> 11140.8 <sup>28</sup> 1112.8 <sup>28</sup>								
01.9998 019080.00.00092.80.009912.90009112.800011171990011115900011192900	01.93338	0.99991	0.00002.8	009912.90	009112:800	0 1 1 101.2900 1	1115.00001	1 922800
1.0000 1113.0 1113.0 1113.0 1113.0 1113.0 1113.0	1.0000	1113.0	1113.0	1113.0	1113.0	1113.0 1	113.0 1	113.0

Table 5: Valus of chi-square and the standard deviation  $\sigma$  for the binary mixtures of DMC with MA, EA and BA at different temperatures.

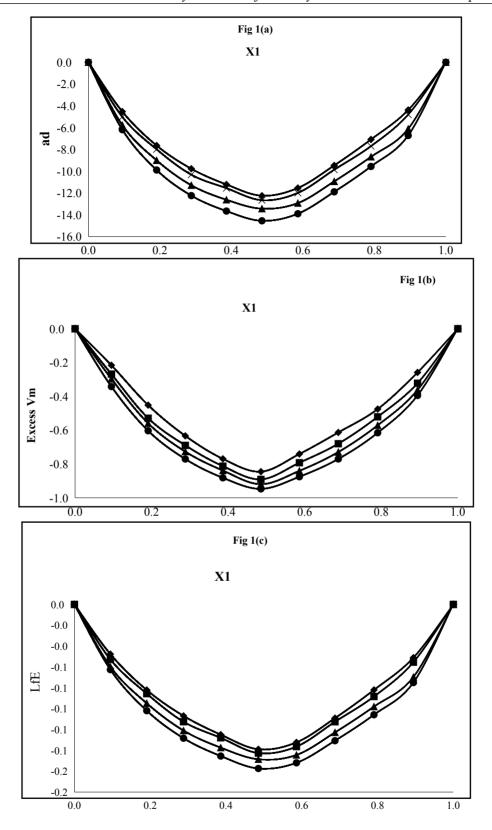
	***************************************				• • • • • • • • • • • • • • • • • • • •					
	UNOM	UNOM Uimp UVDV UJUN		URAO	UKUD					
DMC + Methyl Acetate										
303.15K										
	-0.4798	-0.4508	-0.4779	-0.5184	-0.1544	3.8066				

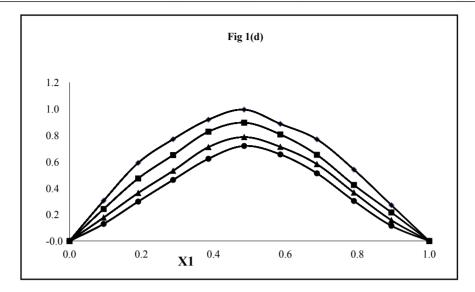
<b>X</b> <sup>2</sup>	30.5319	27.1595	30.2960	35.2974	3.4083	1.5939						
			308.15	K								
	-0.4941	-0.4725	-0.4911	-0.5265	-0.1476	4.0120						
X <sup>2</sup>	31.6775	29.1238	31.3137	35.6975	3.0856	1.7706						
			313.15	K								
	-0.5317	-0.5097	-0.5289	-0.5640	-0.1753	4.3149						
X <sup>2</sup>	35.2559	32.5501	34.9043	39.4212	4.0950	2.0480						
		318.15K										
	0.0485	-0.0107	-0.2491	-0.0569	0.0280	4.4910						
X <sup>2</sup>	0.3653	0.01784	9.14227	0.49645	0.12337	2.21861						
	DMC + Ethyl Acetate											
		303.15K										
	-0.4399	-0.4101	-0.4342	-0.4864	-0.2650	-3.6349						
X <sup>2</sup>	26.4088	23.1860	25.7746	31.8435	9.8829	1.4534						
		308.15K										
	-0.5127	-0.4816	-0.5068	-0.5609	-0.3074	-4.2260						
X <sup>2</sup>	34.1142	30.3620	33.3857	40.3372	12.7680	1.9645						
			313.15	K								
	-0.5869	-0.5572	-0.5809	-0.6342	-0.3478	-4.8311						
X <sup>2</sup>	43.4543	39.4909	42.6406	50.1755	16.0666	2.5674						
			318.15	K								
	0.0485	-0.0107	-0.2491	-0.0569	0.0280	-5.1234						
X <sup>2</sup>	0.3653	0.0178	9.1423	0.4964	0.1234	2.8874						
		DMC	C + Buty	l Acetat	e							
			303.15	K								
	-0.5859	-0.5804	-0.5842	-0.6214	-0.7117	-4.9773						
X <sup>2</sup>	46.1345	45.3527	45.8949	51.4164	65.2205	2.7251						
			308.15	K								
	-0.6949	-0.6925	-0.6944	-0.7292	-0.7896	-5.8268						
X <sup>2</sup>	62.6754	62.2863	62.5892	68.4422	78.4277	3.7347						
			313.15	K								
	-0.7998	-0.7971	-0.7992	-0.8343	-0.8589	-6.6262						
X <sup>2</sup>	80.9863	80.4855	80.8651	87.3650	91.5667	4.8298						
			318.15	K								
	0.0485	-0.0107	-0.2491	-0.0569	0.0280	-7.1010						
X <sup>2</sup>	0.3653	0.0178	9.1423	0.4964	0.1234	5.5467						

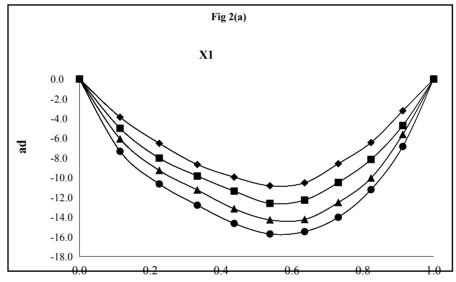
The assumption for the establishment of an ideal mixing relation is that the specific heat ratios of ideal mixtures and volumes are equal. Again, no molecular interactions are taken into consideration. Similarly, the CFT assumes that the molecules are genuine, non-elastic entities, which is not the case. However, when two liquids are mixed, their molecules interact due to the presence of numerous types of forces such as dispersion forces, charge transfer, hydrogen bonding, dipole-dipole, and dipole-induced dipole interactions. Thus, the observed departure of predicted velocity values from practical values indicates that a molecular interaction is occurring between dissimilar molecules in the liquid mixture.

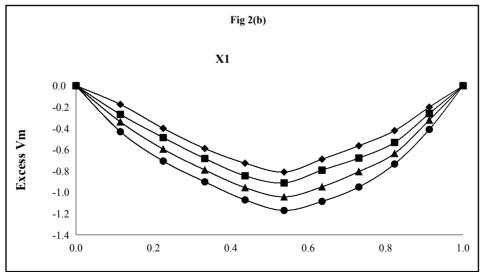
## VI. Conclusion

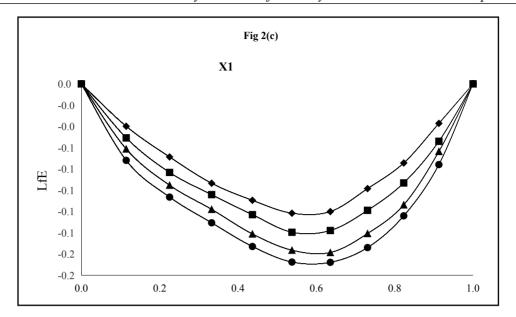
Density,  $\rho$ , and sound speed experimental data are shown, for DMC+MA, +EA, and EA mixes over the whole molefraction range at all studies temperatures T = (303.15 - 318.15) K. Over the whole composition range, excess metrics such as VE,  $\Delta\beta$ ad, LfE and  $\Delta\eta$  were assessed. The results showed that there were intermolecular interactions between DMC and acetate molecules because of their strong hydrogen bonding The DMC - acetate interactions in these combinations are in the following sequence, according to the magnitudes of the excess properties: MA > EA >BA.

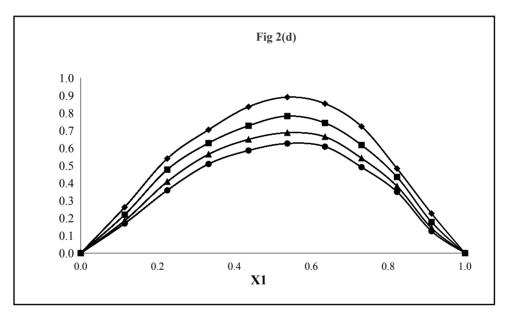


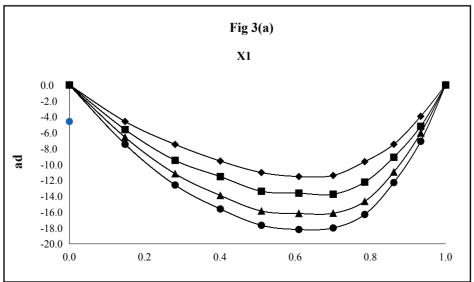


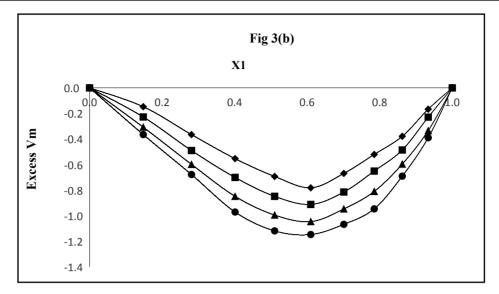


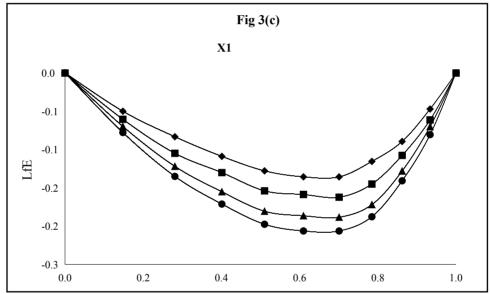


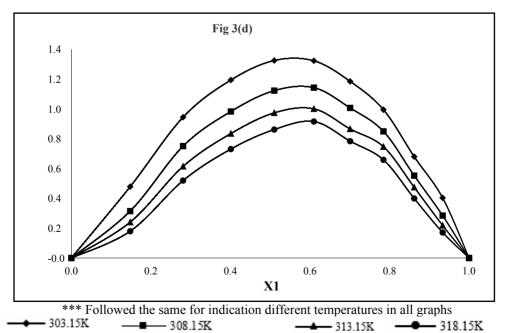












#### **References:**

- A. Gayathri, T. Venugopal and K. Venkata Ramanan, IJ of Engineering & Technology, 2018,7 4.10, 602
- Ganesan, Ravichandran, D. Gopinath, D. Ragouramane, I J of Pure & Applied Physics, 2017, 55(9),664
- [3]. G. Rayichandran, D. Gopinath, S. Armugam, G. Lakshminarayanan, IOSR, Journal of Applied Physics, 2017, 9(3), 51
- O Redlich, AT Kister, Ind Eng Chem. 1948;40:345-8. [4].
- [5]. Nomoto O, J Phys Soc, Japan, 4 (1949) 280 and 13 (1958), 1528.
- Blandamer M & Waddington D, J Phys Chem, 74(1970) 2569. [6].
- Van Dael W & Vangeel E, *Proc Int Conf on calorimetry and thermodynamics*, Warasa (1955) 555. Shipra Baluja & Parsania P H, Asian J Chem, 7 (1995) 417 [7].
- [8].
- Gokhale V D & Bhagavat N N, J Pure Appl Ultrason, 11,1989,pp 21.
- Junjie Z, J China Univ Sci Techn, 14, 1984, pp 298. [10].
- K.Pearson; Fundamentals of Mathematical Statistics, S.G.Gupta, V.K.Kapoor, S.Chand, Company, (Eds.); New Delhi, India, 903
- Reddick J. A, Bunger W.B and Sankano T.K, Organic Solvents 1986,2(4). [12].
- Weissberger A, Proskaner E.S, Riddick J.A & Toops E.E, Organic Solvents, 1955, 2(2).
- [14]. Beebi Sk, Nayeem Sk. Md, Sandhya Sri P.B, Satyanarayana G.R, Zareena Begum+, Rambabu C, J of Thermal Analysis and Calorimetry, DOI 10.1007/s10973-017-6225-4, 2017
- P.B. Sandhya Sri, G.V.Rama Rao, Zareena Begum, M.Krishna Murthy and C.Rambabu, Elixir Appl. Chem. 63 (2013) 18194
- Yadava S.S., Singh Y., Neetu Kushwaha, Global Journal of Molecular Sciences, 2009; 4 (2): 118.
- Murali Krishna Patwari, Ranjith Kumar batchu, Amara Jyothyi Koppula, Satyanarayana Boodida & Satyanarayana Nallani J.Chem Data ,2009; 54: 1069.
- M Karvo. J.Chem Thwermodyn, 1986; 18: 809.
- Fort R.J., Moore W.R, Trans Faraday Soc. 1965; 61: 2102.
- [20]. Gill D.S., Arora D.S., Tewari J., Singh B., J.Chem. Soc., 1988; 84: 1729,
  [21]. Haijum W., Guokang Z, Mingzhi C., J.Chem. Thermodyn., 1993; 25: 949.
  [22]. Ramamurthy M, Sastry O, Indian J Pure Appl Phys, 1983; 21: 579.