Modeling and simulation of pneumatic brake system used in heavy commercial vehicle

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Abstract: An air brake system is used in heavy commercial vehicles for the purpose to stop or slow down the vehicle. The effective braking depends mainly on the response time of the entire system. The brake system layout configuration has to be designed in such a way that the response time should meet the vehicle safety standard regulations. This paper describes the detailed modeling of the individual brake system products, right from the actuating valves, control valves, actuators and foundation brakes. Response time prediction for a typical 4X2 Heavy commercial vehicle has been done. Also a study on comparing the transient torque generated by the existing drum brake and an equivalent disc brake model was carried out. The layout was modeled in one of the commercially available multi-domain physical modeling software employing bond graph technique and lumped system.

Keywords: Response time, AMESim, Multi domain, Foundation brakes, Braking torque

I. INTRODUCTION

The effective braking depends mainly on the response time of the entire system and driver's feel. The response time is determined as the time elapsing between the beginning of the actuation of the control pedal and the moment the pressure in the actuator reaches 75 percent of its asymptotic value[1]. The brake system layout configuration has to be designed in such a way that the response time should meet the vehicle safety standard regulations. The heavy commercial vehicle brake system layout is designed keeping various vehicle parameters like Gross Vehicle Weight, wheel base, Centre of Gravity of the vehicle, number of axles etc. The system layout design is extremely complex since it involves number of valves which have to function in a logical sequence during different stages of braking (Normal, emergency, and One circuit failed condition). Conventionally, the system layout design is arrived after many iterations based on field trials and experience. This method involves more lead time and cost till the layout is finalized. Hence the modeling and analysis of the system layout using AMESim helps us to predict the behavior of the layout in terms of response and the effect of the individual subsystems, valves on the system behavior and thereby optimization study can be carried out. This tool employs bond graph technique and lumped system for developing physical based modeling. Sridhar [2] Describes the modeling of foot brake valve and predicting the dynamic response of the individual valve. Wu [3] studied the robust of pneumatic brake system in commercial vehicle using AMESim. [4], [5],[6] describes the modeling of system by simplifying the valves and the actuators. This paper describes the detailed modeling of individual valves, and actuators by including all the design parameters, thereby makes the model flexible to study the role of each and every design parameter on system level response. Apart from this the paper deals the modeling of foundation brakes and compare the transient torque response of a typical drum and equivalent disc brake for a heavy commercial vehicle. This model can be directly coupled to the vehicle models and the dynamics of the vehicle like stopping distance, stability can be studied. This model can also be used for design and optimization of brake system layouts for various heavy commercial trucks having varying wheel base and Gross Vehicle Weight.

II. AIR BRAKE SYSTEM

A typical Air brake system layout is show in Fig.1, which mainly consist of Compressor (Energy source) Foot/Hand brake valves (Actuating unit) Relay valves (Control unit) and Actuators.
The compressor provides the compressed air, which is the energy source of air brake system. The Air dryer in the layout absorbs the moisture in the pressurized air and also maintains the system pressure. The moisture free compressed air will be stored in the reservoirs through the system protection valve. During normal brake application, when the driver presses the pedal, the dual brake having two deliveries get actuated [1]. The primary delivery gives signal to the relay valve which actuates the spring break actuator where the pressure is converted into braking force. The braking force is transmitted to the foundation brakes through the slack adjuster where it is converted into braking torque and applies brake on the rear wheels. The secondary delivery of the valve actuates the brake chamber thereby applies the brake in the front wheels. In case of emergency situations, the driver actuates the hand valve which applies the brake through the spring brake actuator.

III. MODELING AND SIMULATION

The Air Brake System is modeled using, a commercial tool which has standard libraries for pneumatic, mechanical components. The individual valves, actuators and foundation brakes were modeled using the appropriate elements available in the libraries.

1. Dual Brake Valve

Dual brake valve shown in Fig.2 provides graduated air pressure for applying and releasing of brakes on application of driver’s effort on the brake pedal. The dual brake valve have two independent deliveries, which controls the primary(for rear brakes) and secondary (for front brakes) circuit of the brake system[2]. The design of dual brake valve is such that it ensures uninterrupted supply of air pressure to secondary circuit even in case of primary circuit failure and vice versa.

Based on its geometry and construction the product will be modeled using appropriate mechanical and pneumatic components like piston, spring, and mass available in the library [6].

The flow passages, annular restrictions were modeled as orifices and were introduced in the corresponding location. The mass flow rate of the orifice is governed by equation (1) [7].

\[ m = A C_m C_q \frac{P_{up}}{\sqrt{T_{up}}} \rightarrow (1) \]

where

- \( P_{up} \) - upstream pressure,
- \( T_{up} \) - Upstream temperature,
- \( C_m \) - Mass flow parameter,
- \( C_q \) - Discharge coefficient
- \( A \) - Area of cross section of orifice

The flow coefficient \( C_q \) is introduced to adjust the theoretical relation to experiments. This coefficient is less than one and is used to include extra losses due to local friction and loss of kinetic energy. In all our cases it is assumed as 0.7.

The valves having arrangement as shown in Fig.3 having dynamic flow area is modeled as pneumatic poppet valves, which can accommodate the change in area during valve opening and closing.
The variation in area with respect to valve opening $x$ as shown in Fig. 4 is calculated by using equation (2): 

$$\text{area} = \pi \times ds \times x \rightarrow (2)$$

where

- $x$: Valve lift
- $ds$: Diameter of flapper

The inlet and exhaust valves in primary and secondary were modeled using pneumatic poppet valve model and the flow passages using orifice model. The internal components like piston, springs were modeled using appropriate mechanical and pneumatic elements. The rubber spring used in the brake valve for graduation is assumed to be a linear spring and the complete model is shown in Fig. 5. The signal input to Dual brake valve is given as plunger displacement.

2. Relay Valve

Relay valve is used to speed up the application and release of brakes in case of longer wheel base vehicles. It operates on receipt of signal from the brake valve. The relay valve will graduate, hold, release air pressure from the brake chambers to which it is connected.
It is normally mounted on the rear of the vehicle to balance the brake application time between front and rear. The relay valve consist of a relay piston which get signal from the foot brake valve and controls the opening and closing of inlet and exhaust valve. The piston is modeled using pneumatic piston model and mass element, the inlet and exhaust valves were modeled using the poppet valve model available in the pneumatic library. The flow restrictions through the ports were modeled using the orifice model. The entire relay valve is modeled as shown in Fig.6.

3. Brake Chamber

The brake chamber is the one which generates the braking force in air brake system. It converts the air pressure into mechanical push rod force which engages the brake shoes of the foundation brake system through slack adjuster. The brake chamber consists of a diaphragm which separates the pressure and non pressure side. The diaphragm is held by a spring and push rod assembly and keeps the brake in released position. On application of air pressure the diaphragm moves against the spring and actuates the brake. The diaphragm is assumed to be of having uniform area and is modeled as a piston of constant area. The mass and spring elements were included to model the pushrod and the return spring. The ports were modeled using orifice model. The brake chamber model is shown in Fig.7.

4. Spring Brake Actuator

The spring Brake actuator performs the same as the brake chamber. But it consists of two chambers namely service chamber and spring chamber. The construction and working of the service chamber is same as that of the brake chamber. The spring chamber which is connected to the hand control valve consists of a heavy coil spring. During brake released condition the heavy coil spring will be in compressed position by the air pressure acting on the ram. When the driver actuates the hand valve in case of emergency, the air inside the spring chamber get exhausted and the spring force will actuates the brakes. The spring brake actuator assembly is modeled using appropriate elements as shown in Fig.8.

The diaphragm in the service chamber is assumed as piston of constant area. The other components were modeled using appropriate mechanical and pneumatic elements as shown in Fig.8.
5. Foundation Brake

The foundation brake is the one which converts the actuation force from the actuator into braking torque and stops the vehicle[8]. In India most of the heavy commercial vehicles use drum brakes, which nowadays were being replaced by disc brakes.

5.1 Drum brakes

A drum brake is a brake that uses friction caused by a set of shoes or pads that press against a rotating drum-shaped part called a brake drum. The drum brake and its design parameters were shown in Fig 9. The governing equations for the torque generated by the drum brake is as follows

\[ T = \int \mu r dN = \frac{\mu p_b r^2}{\sin \theta_a} \int \theta_1 \sin \theta d\theta \\
= \frac{\mu p_b r^2 (\cos \theta_1 - \cos \theta_2)}{\sin \theta_a} \rightarrow (3) \]

Figure 9 - Drum Brake and its design parameters

Due to no availability of appropriate element to model the brake shoe the drum brake is modeled using the signal libraries based on equation (3) and is shown in the Fig.10 [9].

5.2 Disc brakes

A disc brake is a wheel brake which slows rotation of the wheel by the friction caused by pushing brake pads against a brake disc with a set of calipers. The disc brake and its design parameters were shown in Fig 11 along with its AMESim model. The disc brake is modeled using the signal library based on the governing equation (4).

\[ M_B = F \times C \times \eta_m \times l \rightarrow (4) \]
6. Creation of Super Components

On completing the modeling of the individual products, the entire system layout needs to be modeled by integrating the models. The models of individual products, having large assembly of components and elements, on integrating to a system level will look complex. For easy representation of these models, the individual product models were shrink and wrap together into a single icon as shown in Fig. 12, called as super component. The input and output ports will be visible in the super component as shown in Fig. 12.

7. Brake system

The super components representing the physical model of the products were integrated using appropriate connections. As our main objective is to simulate the response time of the system, Air dryer, System protection valves which involves in managing the compressed air and system pressure were not considered in the modeling. The hand valve used under emergency application is simplified and modeled as a control signal.

An existing typical 4X2 heavy commercial truck layout has been taken up for modeling. The modeling of system starts from the compressor which is assumed as a constant pressure source. The storage reservoirs were modeled using a fixed volume pneumatic chamber as shown in Fig. 13.
where
\( v \) - Mean gas velocity (m/s)
\( D \) - Diameter of the pipe (m)
\( \Delta p \) - Pressure drop (Pa)
\( L \) - Length of the pipe (m)
\( \rho \) - Density (kg/m³)
\( f_f \) - Friction factor

The reservoir is connected to the supply ports of the brake valve by pipe connection. The rear of the vehicle is having a relay valve. The primary delivery of the brake valve was connected to the relay valve. The delivery of the relay valves was connected to the service side of the spring brake actuators. The secondary delivery of the brake valve was connected directly to the brake chambers in the front axles of the vehicle. Refer Fig. 14. The actuators were connected to the foundation brake model, drum brake (Fig. 14) and Disc Brake (Fig. 15).

The design parameters of the valves and actuators were given and a typical 16 ton vehicle layout with drum brake was taken up for study. The pipe dimensions of the brake system layout were given as input. In the second model (Fig. 15) the drum brakes were replaced with disc brake of equivalent size available in the market.
The driver foot pedal effort was given as plunger displacement of the brake valve. The signal was given such that the total travel of plunger was achieved within 0.2 seconds (Fig.16) as per the vehicle standard requirements [1].

![Figure 17 - Pressure response curve in the spring brake actuator](image1)

The simulation was carried out and the response time was measured by capturing the pressure built-up in the rear, Spring Brake Actuator (least favorable chamber [1]). The pressure response curve was shown in Fig.17 which we got from the Spring brake actuator end. The transient torque generated in both the cases vehicle with drum brake and the same vehicle replaced with equivalent disc brake. Fig.18 shows that on replacing the existing drum brake with equivalent disc brake can generate more torque and can achieve better stopping distance.

![Figure 18 - Pressure response curve in the spring brake actuator](image2)

IV. CONCLUSION

The Brake system model considering all the design parameters was done. A typical 4X2 heavy commercial vehicle having pneumatic brake system with drum brake was taken up for simulation. The response time of the system and the transient torque with drum brake were carried out. The same layout on replacing with an equivalent disc brake shows better torque characteristics. On replacing the drum brake with disc brake the vehicle will have better stopping distance.

The brake system model was flexible enough to study the role of individual valves in system response. Apart from this the model can be further expanded for design and optimization of brake system layout for other heavy commercial vehicle having multi axles. This approach will significantly reduce the overall system design lead time when compared to the conventional method.

Further this can be extended to vehicle modeling along with the foundation brakes and the stopping distance of the vehicle can be simulated.

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