Equilibrium Studies and Kinetics Mechanism for the Removal of Congo red by Passiflora Foetida Activated Carbon–MnO₂- Nano Composite

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Abstract: This paper presents the feasibility of removal of Basic dye (Congo Red) from aqueous solutions by using a low cost PAC-MnO₂-NC. Batch adsorption experiments were carried out as a function of pH, contact time, initial concentration of the adsorbate, adsorbent dosage and temperature. Pseudo first order, Pseudo second order, intra-particle diffusion model and Elovich kinetic models were studied. Thermodynamic parameters such as ∆H°, ∆S°, and ∆G° were also calculated.

Keywords: Congo Red, PAC-MnO₂-NC, Kinetics.

I. Introduction

The textile industries are becoming a major source of environmental contamination, because an alarming amount of dye pollutants are generated during the dying processes [1]. Dye bearing effluent is a significant source of water pollution. Dyes are mainly classified into cationic, anionic and non-ionic dyes. These effluents can cause potential pollutants to human beings and aquatic life. Various physical, chemical and biological separation technologies are used in the removal of these effluents [2]. All of these methods have their own advantages and disadvantages. The method of elimination of dyes using a variety of activated carbon is widely studied, but it was economically expensive [3]. Therefore much interest has focused on methods of adsorption by using natural materials and upgraded wastes [4]. Literature survey shows that various bio adsorbents have been used by researchers such as animal bone [5], black tea leaves [6], cocoa [7], almond shell [8], mango leaves [9], saw dust [10], Jambonut [11], Borassus flabellifer L[12] and Typha Angustata L[13]. Hence adsorption is recommended as a viable means for Basic dye removal. In the present work adsorption capacity of the passiflora foetida plant material [PAC-MnO₂-NC] was studied for the removal of Congo Red at different dye concentration, contact time, temperature, adsorbent dosage, pH and particle size. The adsorption dynamics and thermo dynamic parameters ∆H°, ∆S°, and ∆G° for such systems have been evaluated.

II. Materials And Methods

2.1. Preparation of Activated Carbon

The Passiflora foetida plant materials were collected from local area situated at Thindal, Erode District, Tamilnadu. They were cut into small pieces and dried for 20 days. Finally it was taken in a steel vessel and heated in muffle furnace. The temperature was raised gradually upto 500°C and kept it for half an hour. The carbonized material was ground well and sieved to different particle size. It was stored in a plastic container for further studies. In this study particle size of 0.15 to 0.25mm was used and it was labeled as PAC.

2.2. Preparation of PAC-MnO₂-NC

Activated Carbon (3gm) was allowed to swell in 15mL of water-free Alcohol and stirred for 2 hours at 25°C to get uniform suspension. At the same time, the Managese dioxide (3gm) was dispersed into water-free Alcohol (15mL). Then the diluted Maganese dioxide was slowly added into the suspension of activated Carbon and stirred for a further 5 hours at 25°C. To this, 5mL alcohol and 0.2mL of deionised water was slowly added. The stirring was continued for another 5 hours at 25°C and the resulting suspension was kept overnight in a vacuum oven for 6 hours at 80°C. It was labelled as PAC-MnO₂-NC.

2.3. Preparation of sorbate

Congo red is purchased from S.d. fine chemicals. CR has molecular formula C₃₂H₂₂N₄Na₂O₈S₂. The dye concentration in supernatant solution was determined at characteristic wavelength [λmax =500nm] by double beam UV-visible spectrophotometer [Systronics 2202]. Congo red is the sodium salt of 3,3′-[1,1'-
biphenyl-4,4′-diyl)bis(4-aminonaphthalene-1-sulfonic acid) (molecular weight: 696.66 g/mol). It is a secondary diazo dye. Congo red is water-soluble, yielding a red colloidal solution. The Chemical structure of Congo red is given below.

2.4. Adsorption studies

Batch method was followed by agitating 50 ml of four different dye solutions (10, 20, 30 and 40 mg\textsuperscript{-1}) at their natural pH with 100 mg of PAC-MnO\textsubscript{2}-NC in 150 ml stoppered conical flasks at room temperature (30±2°C) in a temperature controlled water bath shaker at 140 rpm. The samples were withdrawn from the shaker at predetermined time intervals and the dye solution was separated from the adsorbent by centrifuging at 10,000 rpm for 10 min. The absorbance of supernatant solution was measured using UV-VIS spectrophotometer (Cyber Lab, 100) at wave length 500 nm. The amount of CR adsorbed per unit mass was calculated from the following equation:

$$q_t = \frac{(C_o - C_t) V}{W} \hspace{1cm} (1)$$

Where \(q_t\) is the amount of dye adsorbed per unit weight of adsorbent (mg/g); \(C_o\) the initial concentration of CR (mg/L); \(C_t\) the concentration of CR solution at time \(t\) (min); \(V\) the volume of working solution (mL); \(W\) is the adsorbent dosage (mg). Blanks with only the adsorbate in 50 ml of distilled water were conducted simultaneously at similar conditions to account for adsorption in using glass containers. It was found that no adsorption of CR by container walls occurred. The experimental parameters studied are adsorbent dosage, contact time, initial dye concentration, pH and temperature. Adsorption kinetics were tested with pseudo first-order, pseudo second-order, Intraparticle diffusion model, Elovich models.

III. Results And Discussion

3.1. Effects of agitation time and initial dye concentration of dye on adsorption

Effects of agitation time and initial dye concentration (10, 20, 30 and 40 mg/L) on removal of CR are presented in Fig.1. The percent removal of CR increased with increase in agitation time and reached equilibrium at 150 min. The percent dye removal at equilibrium decreased from 71.01 to 54.41 as the dye concentration was increased from 10 to 40 mg/L. It is clear that the removal of dye depends on the initial concentration of the dye. The removal curves are single, smooth and continuous leading to saturation.

Fig.1. Effect of agitation time and concentration of CR on removal of PAC-MnO\textsubscript{2}-NC

3.2. Effect of adsorbent dose

The removal of CR by PAC-MnO\textsubscript{2}-NC at different adsorbent doses are presented in Fig.2. (10mg to 600mg / 50ml) was tested for the dye concentrations 10, 20, 30 and 40 mg/L. Increase in adsorbent dose increased the percent removal of dye which is due to the increase in surface area of the adsorbent.
3.3. Effect of pH

Effects of pH on the removal of CR by PAC-MnO$_2$-NC are shown in Fig. 3. Dye adsorption decreases with increase of pH from 2 to 5 and no remarkable change there after. Low pH favors the adsorption, as decrease of pH the surface become more protonated and acquire positive charge which makes it easier for the anionic dyes to bind with carbon. Poor adsorption of CR at higher pH value is due to the competition between the negatively charged hydroxyl ions and anionic dye for the sorption sites.

3.4. Effect of Temperature

The effect of temperature of adsorption of CR (Fig. 4) for concentration 40 mg/L adsorbent was carried out at 30$^\circ$, 40$^\circ$ and 50$^\circ$C. The percent removal of dye increased from 20.66 to 64.53. This indicates that increase in adsorption with increase in temperature may be due to increase in the mobility of the large dye ions. Moreover, increasing temperature may produce a swelling effect within the internal structure of the adsorbent, penetrating the large dye molecule further.
IV. Adsorption Kinetics

A study of adsorption kinetics is desirable as it provides the information about the mechanism of adsorption, which is important for efficiency of the process. The pseudo first-order, pseudo second-order, Intraparticle diffusion and Elovich adsorption models were used to test dynamical experimental data.

4.1. Pseudo first order model

The linear form of Langergren’s first order rate equation is as follows [14],

\[
\log (q_t - q_e) = \log q_e - \frac{k_1}{2.203} t
\]

where \( q_t \) and \( q_e \) are the amounts of dye adsorbed on adsorbent at equilibrium and at time \( t \), respectively (mg/g) and \( k_1 \) is the rate constant of first order adsorption (min\(^{-1}\)). The slope and intercept of plot of \( \log (q_t - q_e) \) vs \( t \) were used to determine \( k_1 \) and \( q_e \) (Fig 5). These values are shown in Table 1. It is does not fit for pseudo first order kinetics.

![Fig.5. Plot of pseudo first order model at different concentrations](image)

<table>
<thead>
<tr>
<th>Initial Concentration of dye (mg/L)</th>
<th>( q_e ), expt. (mg/g)</th>
<th>( q_e ), cal. (mg/g)</th>
<th>( k_1 ) (mg min(^{-1}))</th>
<th>( R^2 )</th>
</tr>
</thead>
<tbody>
<tr>
<td>10</td>
<td>3.55</td>
<td>1.2133</td>
<td>2.299 \times 10^3</td>
<td>0.947</td>
</tr>
<tr>
<td>20</td>
<td>6.74</td>
<td>2.4322</td>
<td>2.303 \times 10^3</td>
<td>0.963</td>
</tr>
<tr>
<td>30</td>
<td>8.94</td>
<td>2.5061</td>
<td>2.303 \times 10^3</td>
<td>0.960</td>
</tr>
<tr>
<td>40</td>
<td>10.88</td>
<td>3.4434</td>
<td>1.612 \times 10^2</td>
<td>0.968</td>
</tr>
</tbody>
</table>

4.2. Pseudo second order model

The linearised form of the pseudo second order model as given by Ho [15] is

\[
\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e} \quad ...............(3)
\]

where \( k_2 \) is the rate constant of Pseudo-second order adsorption (gm\(^{-1}\) min\(^{-1}\)) and \( q_e \) is the maximum adsorption capacity (mgg\(^{-1}\)). The slope of the plot \( t/q_t \) vs \( t \) gives the value of \( q_e \) and from intercept \( k_2 \) can be calculated (Fig 6). These values are shown in Table 2. It is clear from the nature of fit and correlation coefficients that the adsorption of CR on PAC-MnO\(_2\)-NC is better represented by Pseudo-second order kinetics.
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Fig. 6. Plots of the pseudo-second order model at different concentrations

Table 2: Pseudo second order Kinetic Parameters for the adsorption of CR by PAC-MnO₂-NC at various concentrations

<table>
<thead>
<tr>
<th>Initial Concentration of dye (mg/L)</th>
<th>qₑ expt. (mg/g)</th>
<th>Pseudo Second-order Kinetics</th>
<th>qₑ cal. (mg/g)</th>
<th>k₂ (mg min⁻¹)</th>
<th>R²</th>
</tr>
</thead>
<tbody>
<tr>
<td>10</td>
<td>3.55</td>
<td>3.6231</td>
<td>0.6275x10⁻¹</td>
<td>0.6275x10⁻¹</td>
<td>0.999</td>
</tr>
<tr>
<td>20</td>
<td>6.74</td>
<td>6.9444</td>
<td>2.236x10⁻²</td>
<td>2.236x10⁻²</td>
<td>0.999</td>
</tr>
<tr>
<td>30</td>
<td>8.94</td>
<td>9.1743</td>
<td>2.176x10⁻²</td>
<td>2.176x10⁻²</td>
<td>0.999</td>
</tr>
<tr>
<td>40</td>
<td>10.88</td>
<td>11.2359</td>
<td>1.0791x10⁻²</td>
<td>1.0791x10⁻²</td>
<td>0.999</td>
</tr>
</tbody>
</table>

4.3. Elovich kinetic model

A simplified linearized form of Elovich kinetic equation [16] is presented as follows:

\[
q_t = \frac{1}{\alpha} \ln(\beta t) + \frac{1}{\alpha} \ln(t)
\]

where \(\alpha\) is the initial adsorption rate (mg/g/ min), \(\beta\) is the desorption constant (g/mg) during any one experiment.

A plot of \(q_t\) versus \(\ln(t)\) with a straight line, as expected, with a slope of \((1/\beta)\) and an intercept of \((1/\beta)\ln(\alpha\beta)\) can be calculated in Fig.7. The elovich model parameters \(\alpha\), \(\beta\) and correlation coefficient \(R²\) are summarized in Table 3. From the table the initial adsorption rate \((\alpha)\), desorption constant \((\beta)\) and the correlation coefficient \((R²)\) are calculated. The correlation coefficient is \((R²)\) is less than that of Pseudo second order model.

Fig.7. Elovich kinetic model of CR by PAC-MnO₂-NC
4.4. Intraparticle diffusion model
The intra particle diffusion model is used here refers to the theory proposed by [17] the following equation for the rate constant:

\[ q_t = k_{id} t^{0.5} + C \]  \hspace{1cm} (5)

Where \( k_{id} \) is the intra particle diffusion rate constant (mg/g min\(^{1/2}\)) and C is constant. If that rate limiting step is intra particle diffusion, the graphical representation of adsorbed dye \( q_t \) versus \( t^{0.5} \) yield straight lines passing through the origin and the slope gives the intra particle diffusion rate constant \( k_{id} \) and correlation coefficient \( R^2 \) is indicated in Fig. 8.

![Graph showing the intraparticle diffusion model for CR by PAC-MnO\(_2\)-NC](image)

Fig. 8. Intraparticle diffusion model kinetic model of CR by PAC-MnO\(_2\)-NC

The intra-particle parameters \( k_{id}, C \) and correlation co-efficients \( R^2 \) are summarized in Table 3. From these data inter set value indicate that the line are not passing through origin, therefore some other process that may affect the adsorption. The correlation coefficient \( (R^2) \) value is less than that of Pseudo second order model.

Table 3: Elovich and Intraparticle diffusion Model of CR by PAC-MnO\(_2\)-NC

<table>
<thead>
<tr>
<th>Initial Dye Concentration (mg/L)</th>
<th>Elovich Model</th>
<th>Intraparticle diffusion Model</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>( \beta )</td>
<td>( \hat{R}^2 )</td>
</tr>
<tr>
<td>10</td>
<td>142.864</td>
<td>3.1645</td>
</tr>
<tr>
<td>20</td>
<td>56.8092</td>
<td>1.4224</td>
</tr>
<tr>
<td>30</td>
<td>2162.26</td>
<td>1.1976</td>
</tr>
<tr>
<td>40</td>
<td>48.2067</td>
<td>0.8264</td>
</tr>
</tbody>
</table>

Adsorption kinetics and isotherms are very important information for adsorption process design. Compared with the pseudo-first order, Elovich, Intraparticle diffusion model, the pseudo-second order kinetic model was found to fit the dye adsorption kinetic data more appropriately. Although many different adsorbents are tried to remove dyes from wastewaters, activated carbon from various sources is still the most widely used adsorbent for color removal.

V. Thermodynamic Parameter

Thermodynamic parameters like \( \Delta H^* \) and \( \Delta S^* \) were evaluated using Van’t Hoff’s equation:

\[ \ln K_c = \frac{\beta S^*}{R} - \frac{\beta H^*}{RT} \]  \hspace{1cm} (6)

Where \( K_c \) is the Langmuir equilibrium constant, \( \Delta H^* \) and \( \Delta S^* \), are the standard enthalpy and entropy changes of adsorption respectively and their values are calculated from the slopes and intercepts respectively of the linear plot of \( \ln K_c \) Vs 1/T. The free energy change for the adsorption process \( \Delta G^* \) (kJ/mol) is derived in equation 7.

\[ \Delta G^* = \frac{\Delta H^*}{T} - \Delta S^* \]  \hspace{1cm} (7)

The values of these parameters were calculated using equation (6&7) at various initial Concentrations and are shown in Table 4.

Table 4: Thermodynamic parameters for the adsorption of CR by PAC-MnO\(_2\)-NC

<table>
<thead>
<tr>
<th>( \Delta G^* ) (kJ/mol)</th>
<th>303K</th>
<th>313K</th>
<th>323K</th>
<th>333K</th>
<th>( \Delta S^* ) (J/mol/K)</th>
<th>333K</th>
<th>( \Delta H^* ) (kJ/mol)</th>
</tr>
</thead>
<tbody>
<tr>
<td>303K</td>
<td>31.31</td>
<td>32.31</td>
<td>33.33</td>
<td>33.33</td>
<td>83.8882</td>
<td>25.9396</td>
<td></td>
</tr>
</tbody>
</table>
The adsorption data indicates that $\Delta G^o$ were negative at all temperatures. The negative $\Delta G^o$ confirms the spontaneous nature of adsorption of CR by PAC-MnO$_2$-NC. The magnitude of $\Delta G^o$ suggests that adsorption is physical adsorption process. The positive value of $\Delta H^o$ were further confirms the endothermic nature of adsorption process. The positive $\Delta S^o$ showed increased randomness at the solid-solution interface during the adsorption of CR dye by PAC-MnO$_2$-NC. This was also further supported by the positive values of $\Delta S^o$, which suggest that the freedom of CR is not too restricted in the adsorbent, confirming a physical adsorption. The $\Delta G^o$ value increases with increase in temperature is the increase in enhancement of the adsorption capacity of adsorbent may be due to increase or enlargement of pore size and/or activation of the adsorbent surface.

VI. Desorption Studies

After activated carbon is saturated with dye molecules, different solvents could be used to regenerate the activated carbon to restore its dye adsorptive capability [18]. Desorption with acetic acid revealed that the regeneration of adsorbent was satisfactory, which confirms the physisorptive nature of adsorption.

VII. Conclusions

The present study shows that PAC-MnO$_2$-NC is an effective adsorbent for the removal of CR from aqueous solution. The thermodynamic parameters were found to be thermodynamically favourable physical adsorption process. Evaluation of thermodynamic parameters showed the process as endothermic and spontaneous. The kinetic parameters fit for Pseudo second order model. Desorption studies reveals that satisfactory desorption taking place confirming physisorptive nature of adsorption. Complete removal of the dye can be achieved using an appropriate dosage of the adsorbent and pH for waste waters. The results would be useful for the fabrication and designing of waste water treatment plants for the removal of dye. Since the raw material is freely available in large quantities the treatment method, seems to be economical.

References


